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# ESSA Technical Report ERL 177-SDL 15

U.S. DEPARTMENT OF COMMERCE  
Environmental Science Services Administration  
Research Laboratories

## SIXBIT A Generalized Reaction Kinetics Program

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BOULDER, COLO.  
AUGUST 1970



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## ESSA TECHNICAL REPORT ERL 177-SDL 15

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## SIXBIT - A GENERALIZED REACTION KINETICS PROGRAM

G. W. Adams and L. R. Megill

A FORTRAN-IV computer program, SIXBIT, has been written as a general reaction-handling tool. This report describes the use of SIXBIT as a "black-box" program, and describes the program in detail.

Key Words: atmosphere, chemistry, computer, differential equations, program, reactions.

### 1. INTRODUCTION

In the past few years a number of computer programs designed to solve sets of coupled, time-dependent differential equations, describing the behavior of a set of reactants, have been written. See, for example, Keneshea [1962, 1963, 1967] and Hunt [1966]. The justification for writing yet another of these programs is as follows.

Past programs have been relatively inflexible, requiring rather major reprogramming to vary the set of reactants. In addition, it is often difficult to determine the major process operating in a complicated system. SIXBIT attempts to resolve these two difficulties.

The first objective is answered by subroutine ALGEBRA, which takes a series of cards describing the reactions and writes the appropriate set of differential equations. Once a basic set of reactions is given to the program, adding or deleting one or two reactions is a trivial task.

The second objective is more difficult to answer. An attempt to get out the pertinent information is made by printing out a table giving the major production and destruction mechanisms for each species.

These two features make the program a useful tool for ionospheric research and perhaps for some laboratory investigations. Of necessity,

a number of approximations have been made in handling the solar flux in the atmosphere. The succeeding pages specify those approximations. In addition, no diffusive processes have been included. There are, of course, a significant number of problems in which this omission will make the results invalid.

Extensive measures have been taken both to maintain the accuracy and to keep track of a parameter describing the accuracy of the calculations. The program automatically adjusts the step size as needed to keep the accuracy up. This allows for a great increase in speed, since we find that the step size may change from as short as a few microseconds during twilight to steps of the order of an hour in the middle of the day or night. The resulting program has turned out to be quite fast.

Another feature of the program is that the sun can be "held" in a single position (e.g., noon) while the program is run to steady state. This allows starting values to be obtained so that diurnal variations may be calculated without a steady drift in value of species that have time constants long with respect to a day.

The program is written in FORTRAN IV as used at the Boulder Laboratories CDC 3800. This language allows extensive indexing of indices which is not allowed on many FORTRAN IV systems. However, at least some versions of FORTRAN V allow this flexibility. No extensive measures have been taken to trap for overflows and underflows, and attempts to use this program on machines allowing exponent ranges of  $\pm 38$  may result in difficulties

The program as presently dimensioned will take 50 reactions, 20 reactants, and 20 heights. These limitations are not fundamental and can easily be extended by modifying dimension statements. The emphasis in this work, however, is to concentrate on the physical processes operating in a system and it is felt that more reactions than this may be exceedingly difficult to interpret.

This report is in two sections. Section 2 describes the use of the program as a "black box." This involves the use of the program without reference to its internal workings. Section 3 describes the program in detail sufficient for the person who may want to modify it.



## 2. USING SIXBIT

### 2.1 Data Input

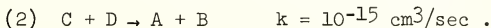
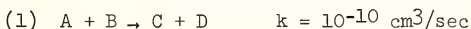
(Appendix A is the listing of one of the data decks actually used for the calculations described in Section 3.)

A. The first input card contains a single integer; 0 or 1. A 0 tells the program to take all the input data from the data cards. A 1 picks up the species concentrations from a magnetic tape, where they were written out in a previous run, but gets the rest of the data from cards. This restart capability is particularly useful on computer systems with restrictive running times.

B. The second card also contains a 0 to 1. A 1 tells the program to make microfilm plots of the profiles; 0 tells it not to.

C. The next three cards contain an alpha-numeric note to yourself so you can remember what you are doing. These three cards will be printed out as the first output of the program.

D. Reactions. Write down on paper your complete reaction set, and make a list of all the species involved. Number the species consecutively. 1 and 2 are not used as species numbers; these are preempted by the program. 3 is  $O_2$  and 4 is  $O_3$ . From 5 on, there is no restriction on the species identities. If your reaction set uses  $O_2$  and/or  $O_3$ , use these numbers for them. Otherwise, start your numbering with "5". In either case,  $O_2$  and  $O_3$  profiles will be printed out. Now, rewrite your reaction set in terms of the species numbers, making one list for the regular reactions and a second list for the photoreactions. Each reaction must appear in the form of 3 body  $\rightarrow$  3 body, so anywhere you have blanks, enter a "1". As an example, consider the reaction set



Assuming that neither  $O_2$  nor  $O_3$  is part of this set, we would number the species  $A = 5$ ,  $B = 6$ ,  $C = 7$ ,  $D = 8$ . Then the reactions would be

- (1) 05 + 06 + 01 → 07 + 08 + 01  
 (2) 07 + 08 + 01 → 05 + 06 + 01 .

Now express each rate coefficient in the form

$$k = k_0 \left(\frac{T}{A}\right)^n e^{B/T}$$

where  $k_0$ ,  $A$ ,  $n$ , and  $B$  are constants, and  $T$  is temperature. (The temperature is entered later.) If the rate coefficients are just constants, as in the example, you would have for the first reaction  $k_0 = 10^{-10}$ ,  $A = 1.0$ ,  $n = 0$ ,  $B = 0$ . Note that  $A$  must not = 0, since it is used as a divisor. However, with  $n = 0$ , any positive value of  $A$  will do equally well. The (non-photo-) reactions can now be card-punched, one reaction (with rate coefficient) to a card. There can be any number of reactions up to a maximum of 50. (This number is limited only by the dimension size in the program or the machine memory size and is not fundamental.) In order for the program to know when all the reactions have been read in, the last card in this set must have a "99" punched in columns 1 and 2, with the rest of the card blank. The reaction set will be printed out when the program is run.

FORMAT (3(I2,1X),1X,3(I2,1X),6X,2(E8.2,2X),2(E9.2,2X))

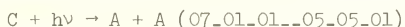
SAMPLE ( / IS EDGE OF CARD)

/05-06-01--07-08-01-----1.00E-10--1.00E+00--+0.00E+00--+0.00E+00  
 /07-08-01--05-06-01-----1.00E-15--1.00E+00--+0.00E+00--+0.00E+00

E. Photoreactions. The photoreactions now exist in terms of the species numbers. For these, the reaction cross sections as a function of wavelength must be specified. SIXBIT works with the wavelength region  $0 \leq \lambda \leq 12,000\text{\AA}$  in  $100\text{\AA}$  steps, numbered as

- 1 = 0 -  $100\text{\AA}$   
 2 = 100 -  $200\text{\AA}$   
 3 = 200 -  $300\text{\AA}$   
 . . . . .  
 120 = 11,900 -  $12,000\text{\AA}$  .

For each reaction, you must specify (a) the number of the first wavelength region with non-zero cross-section, (b) the number of the last region with non-zero cross-section, and (c) the cross-section for each region. To our example reaction set, add the photoreaction



with a cross-section which is  $10^{-19} \text{cm}^2$  in the region 1850-2400Å and is zero elsewhere. Then we would specify 19 and 24 as the first and last wavelength regions, followed by  $5 \times 10^{-20}$  and five  $1 \times 10^{-19}$ . The first cross-section has been adjusted to give the average cross-section over the region 1800-1900Å. The photoreaction list can contain any number of reactions up to a maximum of 20. It must be terminated with a "99" just like the reaction list was.

```
FORMAT (3(I2,1X),1X,3(I2,1X))
```

```
FORMAT (I3,2X,I3)
```

```
FORMAT (7(E8.2,2X))
```

```
SAMPLE
```

```
/07_01_01--05_05_01
```

```
/019_024
```

```
/5.00E-20--1.00E-19--1.00E-19--1.00E-19--1.00E-19--1.00E-19
```

Notice that both here and in the calculation of the photon attenuation, which is handled separately, 100Å bands are used. This will lead to problems any time the cross-sections have structure, since there is no way to average across such structure and still obey Beer's Law. There are several ways this problem can be handled, but it is left to the user to find a reasonable way to treat any particular case.

F. Altitude Information. Altitudes are in kilometers, with the highest one first. There are two ways to get this information in.

1. Constant height interval. This is denoted by the first number (an integer) being 0. The next three numbers are the highest altitude, the lowest altitude, and the height interval. For example, if you want 30-100 km in 5-km intervals, you punch 0 (to tell it it's constant height interval), then 1.000E+02, 3.000E+01, 5.000E+00.

2. Non-constant height interval. The initial integer is the number of heights to be given, followed by the altitude values in descending order.

For either form of input, a maximum of 20 altitude values is allowed by the present dimension sizes.

```
FORMAT (I2,6(2X,E9.3)) - FIRST CARD
FORMAT (6(E9.3,2X)) - ALL OTHER CARDS
SAMPLE NO. 1 (CONSTANT STEP SIZE)
/00_1.000E+02_3.000E+01_5.000E+00
SAMPLE NO. 2 (VARIABLE STEP SIZE)
/04_1.000E+02_9.500E+01_9.000E+01_8.000E+01
```

G. Temperature Profile. One value of temperature must be given for each altitude, starting with the highest altitude. If none of the rate coefficients has any temperature dependence, then any non-zero values can be entered here.

```
FORMAT (7(E8.2,2X))
SAMPLE
/1.23E+02_1.37E+02_1.46E+02_1.70E+02
```

H. Number of Atoms per Species. The easiest way to maintain accuracy in a calculation like this is to calculate all the densities except one, then determine what that one must be to keep the total number of atoms/cm<sup>3</sup> a constant. Unless the errors get so large that one of the densities goes negative, you will never know anything about the accuracy this way. A better way is to calculate all the densities, then multiply them all by a factor which will keep the total number of atoms/cm<sup>3</sup> a constant. As long as this factor is reasonably close to unity at each step, this approach appears to do well at keeping errors from growing. However, this only controls the total number of atoms, so that oxygen can get converted to nitrogen (for example) and still keep the total number of atoms constant. Therefore, the procedure in SIXBIT is to determine all the different types of atoms which should keep their total numbers/cm<sup>3</sup> constant, such as hydrogen, oxygen, etc. Order these types so that the least abundant one is first and the most abundant one is last. For each species,

the number of each different type of atom is given. Every print-out time, SIXBIT will (1) determine the total number of atoms/cm<sup>3</sup> of the least abundant type, (2) determine the multiplicative factor required to get the total back to the total that was input, (3) multiply those densities which contain that type of atom by this factor, (4) determine the total number of atoms/cm<sup>3</sup> of the next least abundant type, etc. Normally the most abundant type of atom will be the total of all types of atoms. Each time a new factor is determined and used to multiply one of the sets, species #2 will also be multiplied by the factor. Species #2 starts with a value of 1 at all altitudes, and nothing else happens to it. It gets printed out with the other densities, and thus reflects the total amount of "squeezing" that has occurred at each altitude.

FORMAT (I2,2X,10(I1,1X))

SAMPLE

/07--2\_1\_0\_0\_1\_0\_4

I. Time and Miscellaneous Flags. This consists of one card containing 9 numbers.

1. T, the reaction time relative to the time at which the calculations were started. This is normally input as zero, although it is sometimes convenient to change it when a reaction set is being restarted. Its only essential use for you (although not for the program) is to keep track of time for reaction sets with characteristic times of less than a second.

2. TPRINT, the time interval for which you want the data printed out. This number will automatically be adjusted by the program. If you tell it to print out every second (TPRINT = 1.0), then it will print out the results of the calculations every second for 10 seconds. At this point it will examine the average time steps that the program used in the last print-out intervals. If the

minimum step-size is greater than  $\text{TPRINT} \times 10^{-3}$ , then TPRINT will be multiplied by 10. TPRINT will continue to be increased by factors of 10 at 100 seconds, 1000 seconds, etc., up to a maximum (see below), as long as the step-size continues to grow (the normal circumstance for most reaction sets).

3. The solar zenith angle and the photon fluxes are recalculated only at print-out time. For this reason, you do not want TPRINT to get too large. TMAX1 is the maximum value that TPRINT is allowed to have when the sun is above the horizon or when the region of the atmosphere for which you are doing calculations is in total darkness. A reasonable value here is 1 hour ( $3.6 \times 10^3$ ) for calculations of diurnal variations.

4. TMAX2 is the corresponding upper limit for TPRINT during twilight. One minute is reasonable here, unless you are running to steady state.

5. TQUIT is the stopping time for the program (in seconds). Typically this might be several days ( $1 \text{ day} = 8.64 \times 10^4$  seconds).

6. IFLAG8 chooses between two methods of solution. A 0 chooses a standard fourth-order Runge-Kutta routine with variable step-size. A 1 chooses a partial integration routine. The choice depends on the type of reaction set you are dealing with. Basically, if the rapidly varying species are minor (relatively low concentration) species in a "sea" of relatively stable major species, then the partial integration routine is usually faster. If the major species are also the rapidly changing species, then the Runge-Kutta routine is usually faster. Most atmospheric problems will therefore run best with the partial integration routine,

while the two-reaction set we have been using for an example will be fastest with Runge-Kutta.

7. IFLAG1 is an integer that controls whether or not species can go into steady state. A 1 here lets species go into steady state when they satisfy the criteria (input later on this card). A 0 does not let species go into steady state.

8. EQUIL is the criterion for letting species go into steady state. If X is the species concentration, then X will go into steady state (assuming it's allowed to go by IFLAG1) if

$$\frac{1}{X} \frac{dX}{dt} < \text{EQUIL}$$

$10^{-8}$  is a reasonable value for EQUIL.

9. JOSHUA controls the motion of the sun. If JOSHUA = 0, the sun will go through its normal diurnal variation. If JOSHUA = 1, the sun will remain stationary in the sky. This is used to get steady-state starting values for a reaction set by holding the sun at noon and running to steady state.

FORMAT (5(E8.2,2X),2(I1,2X),E8.2,2X,I1)

SAMPLE

/0.00E+00\_\_1.00E+00\_\_3.60E+03\_\_6.00E+01\_\_8.64E+05\_\_0\_\_1\_\_1.00E-08\_\_0

J. Local Time Information. This card contains

1. LAT = latitude in degrees
2. LONG = longitude in degrees
3. TMONTH = number of the month
4. TDAY = day of the month

5. THOUR = local hour
6. TMIN = local minute
7. TSEC = local seconds

```
FORMAT (2(E9.2,2X),5(I2,2X))
SAMPLE
/+3.72E+01__+9.25E+01__03__05__23__00__00
```

K. Starting Species Concentration Profiles. The initial value of each species concentration at each altitude can be specified, but not all of them have to be. If  $O_2$  and  $O_3$  (#3 and #4) are not input, internal profiles will be used. However, all altitudes must be in the range 30-200 km to use this feature. Any other species profile not specified will be taken as  $5 \times 10^{-6}$  times the  $O_2$  concentration. (This is somewhat faster than starting the calculations with zeroes.) The species member is entered on a card by itself; the altitude profile is entered on the following card. This set must be terminated with a "99" in the first two columns, as before.

```
FORMAT (I2) - FIRST CARD - SPECIES NUMBER
FORMAT (7(E8.2,2X)) - FOLLOWING CARDS - ALTITUDE PROFILE
SAMPLE
/04
/9.37E+08__4.25E+09__8.34E+09
```

## 2.2 Program Output

(See Appendix B for a sample)

### A. Information Output Only at the Beginning

1. The three alphanumeric cards you input will be printed out.
2. A statement telling how many reactions (excluding photo-reactions) and how many species you input is printed. (If



your highest numbered species is 13, then you put in 11 species, since species numbering starts with #3.)

3. A list of the reactions and rate coefficients that you input, numbered sequentially in the order you put them in.

4. The number of photo-reactions input.

5. A list of the photo-reactions, numbered sequentially from the reaction set.

6. A label which says "Starting Values".

7. The local time as you input it.

8. The amount of computer time used up to this point.

9. The reaction time (T) as you input it.

10. The zenith angle of the sun.

11. A table labeled "Reaction Terms" containing, at this point, the rate coefficients for the reactions as a function of altitude.

12. A table labeled "Species Densities" containing the profiles you input, plus the density for species #2, which is 1.0 at this point.

B. Information Output Every Print-Out Time

1. Local time, as above.

2. Total computer time used up to this point.

3. T, the reaction time in seconds relative to the starting point.

4. The solar zenith angle which was used during the last step, therefore the zenith angle appropriate to the previous time, not to the present time.

5. A table labeled "Reaction Terms." For the reaction



with rate coefficient K, the reaction term is

$$K[A] [B] [C] .$$

In other words, the reaction term is the absolute value of the contribution to the time derivative of species A, B, C, D, E, or F due to this particular reaction. Another interpretation is that it is the number of times per second that this particular reaction is occurring.

Note that the first entry at each altitude in this table is the average step-size in seconds used by the program over the previous print-out interval.

6. A table labeled "Species Densities". Self-explanatory. A minus sign in front of a density indicates that the species is in steady-state. A minus sign in front of an altitude means that all species at that altitude are in steady state.

7. A table labeled "Major Destruction Reactions". For each species at each altitude, a survey is made of all the reactions to see which is the major destroyer. This reaction number is printed out, followed by a slash and then the numbers of the next three destroying reactions, provided that each of the next three is within a factor of 10 of the biggest destroyer. A

"1" indicates that there are no non-zero destroying reactions for that species. A "-0" indicates that there is no such species.

8. A table labeled "Major Production Reactions". As above.

### 2.3 Other Things

The program can make microfilm plots of the altitude profiles at each print-out time. Figure 1 shows a sample plot. For local users, the card in subroutine MICROPLT which gives user's name and extension will have to be changed. For other users, subroutine MICROPLT and the CALL MICROPLT statement in the main program (SIXBIT) will have to be removed.

The profiles are written out on tape unit 13 every print-out and then 13 rewinds, so that the last profile is always available. Having the first card input value =1 lets the program read starting profiles, but not the rest of the data, from tape. A dummy read statement is the very first operation in SIXBIT. Therefore, to get started, remove that initial read statement for the first run so that the tape gets labeled, then replace the read statement so that you are always initially reading a labeled tape.

If you find any bugs in the program, please let us know. For people on other machines --We would appreciate learning what machine you are running on and what changes you find need to be made for your machines. This will be helpful to other people using similar machines.

### 3. THE INTERNAL WORKINGS OF SIXBIT

#### 3.1 Variable Definitions

(Appendix C is a complete listing of the program.)

##### A. Indices

I - reaction number, goes from 1 to NREAC.

II - photoreaction number, goes from 1 to NFREAC.

IJZ - reaction rate constant index for reaction I at altitude JZ, goes from 1 to (I)(JZ).

ILOOK - searching index used in PHYSICS, goes from 1 to 4.

ITCH - type-of-atom index, goes from 1 to ITCHXX.

JRK - Runge-Kutta index, goes from 1 to 4.

JZ - altitude number, goes from 1 to JZEND.

JZTAB - altitude index used for tabulated values of  $O_2$  and  $O_3$ . Runs from 1 to 87, corresponding to altitudes of 200-28 km in 2-km steps.

LAMDA - wavelength number, goes from 1 to 120 corresponding to wavelength bands 0-100Å, 100-200Å, etc., up to 11,900-12000Å.

M - species number, goes from 1 to NSPEC.

##### B. Dimensioned Variables (All contained in COMMON /A/)

A(I) - Input, read and used in ALGEBRA, part of the temperature-dependent rate coefficient,  $K = K_0 \cdot (TEMP/A)^{**N} \cdot EXPF(B/TEMP)$ . Should never be zero, since it's used as a divisor.

ARK(JRK) - one of the sets of constants (set in START) used in the Runge-Kutta technique.

B(I) - See A(I).

BRK(JRK) - See ARK.

CRK(JRK) - See ARK.

F(M) - The sum of all gain terms for Y(M), so that the differential equation is written  $\frac{dY(M)}{dt} = F(M) - G(M)*Y(M)$  where  $F(M) \geq 0$  and  $G(M) \geq 0$ . Includes both terms from regular reactions and terms from photoreactions.

FF(M) - Same as F(M) evaluated  $\Delta t = H$  later. Used to calculate backwards in time to see if the species densities return to where they started.

FLUX(LAMDA) - The photon flux (photons/cm<sup>2</sup>-sec-100 Å) calculated at a particular altitude and zenith angle. Calculated in PRODUC.

FLXINF(LAMDA) - The photon flux (photons/cm<sup>2</sup>-sec-100 Å) outside the atmosphere. Tabulated in table 1, plotted in figure 2. Set in a DATA statement in START.

FRATE(II) - The cross-section times the photon flux, summed over wavelength, for the IIth photoreaction. FRATE times the species density Y(LLL(II)) gives the number of times per second that the reaction goes. Calculated in PRODUC, used in WEIRD.

FTERM(II) - FRATE(II)\*Y(LLL(II)), one of the photo-terms which gets added up to form the differential equations.

G(M) - The sum of all loss terms for Y(M). See F(M).

GG(M) - G(M) evaluated at  $t + H$ . See FF(M).

HBAR(M) - The average step-size over the previous print time. Used in WEIRD to get an initial value for H, and printed out.

H2HOLD(JZ) - The scale height of O<sub>2</sub> at a particular time. Calculated in ZENANG from the O<sub>2</sub> profile; used in PRODUC.

H3HOLD(JZ) - Same as H2HOLD but for O<sub>3</sub>.

IATOM(ITCH,M) - The number of atoms of type ITCH per molecule, for species M, used to determine the total number of atoms per cm<sup>3</sup> as an error check. Input.

IGAIN(ILOOK) - The numbers of the reactions which are the dominant gain processes for a particular species at a particular altitude. This gets transferred to IGAINA, B, C, or D. Determined in PHYSICS.

IGAINA(M,JZ) - The reaction which is the biggest producer of species M at altitude JZ. This will be set = -1 if there are no producers (this is possible since PHYSICS does not look at photoreactions), and = 0 if there is no such species. This gets calculated in PHYSICS and is part of the program's output.

IGAINB(M,JZ) - The reaction which is the second biggest producer of species M at altitude JZ, provided it's within a factor of 10 of IGAINA. See IGAINA.

IGAINC(M,JZ) - The third biggest producer of M at JZ. See IGAINB.

IGAIND(M,JZ) - The fourth biggest producer of M at JZ. See IGAINB.

ILOSS(ILOOK) - The dominant loss processes for a particular species at a particular altitude. This gets transferred to ILOSSA, B, C, or D. See IGAIN.

ILOSSA(M,JZ) - The reaction which is the biggest destroyer of species M at altitude JZ. See IGAINA.

ILOSSB(M,JZ) - Loss equivalent of IGAINB.

ILOSSC(M,JZ) - Loss equivalent of IGAINC.

ILOSSD(M,JZ) - Loss equivalent of IGAIND.

INFORM(INFO) - 30 words of information to yourself. Three cards of alphanumeric reminders which get written out at the first of a run. Read in SIXBIT.

JPULL(JZ) - A flag set to 1 is all species are in steady state at altitude JZ; = 0 if they are not. Calculated in SIXBIT.

K(IJZ) - The rate coefficient for reaction I at altitude JZ. See A.

K0(I) - The constant (non-temperature-dependent) part of K. See A.

KABS(II,LAMDA) - The input absorption cross-section for the IIth photo-reaction. Read in REACTS, used in PRODUC to calculate FRATE.

KABSN2(LAMDA) - The absorption cross-section for N<sub>2</sub>, in cm<sup>2</sup> (100 Å)<sup>-1</sup>. Set by a DATA statement in START. Plotted in figure 3, tabulated in Table 1.

KABS02(LAMDA) - The absorption cross-section for O<sub>2</sub>, in cm<sup>2</sup> (100 Å)<sup>-1</sup>. Tabulated in Table 1; plotted in figure 3. Set by a DATA statement in START; used in PRODUC to calculate FLUX. Taken from Allen [1963].

KABS03(LAMDA) - The absorption cross-section for O<sub>3</sub>, given in Table 1 and figure 4. See KABS02.

KRK(MJRK) - The four first derivatives for each species calculated for the Runge-Kutta solution.

L1(I) - The number of the first species on the left-hand side of the Ith reaction. Input, read in REACTS.

L2(I) - The second species on the left-hand side of the Ith reaction.

L3(I) - The third species on the left-hand side of the Ith reaction.

LL1(II) - The first species on the left-hand side of the IIth photoreaction.

LL2(II) - The second species on the left-hand side of the IIth photoreaction.

LL3(II) - The second species on the left-hand side of the IIth photoreaction.

N(I) - See A.

NASRAS(M\*I) - The Number And Sign of the Reaction Affecting the Species. A long array, divided up into a region for each species. Each region contains the reaction numbers of all reactions which are destroyers of that species, and reaction number + NREAC for all reactions which are producers of that species.

NFTERM(M) - The number of photoreactions which involve the Mth species calculated in ALGEBRA.

NTERM(M) - The number of reactions which involve the Mth species.

NUSRUS(M\*II) - The number and sign of the photoreaction affecting the species. See NASRAS.

PHOLD(M,JZ) - An integer array which contains a "1" if species M at altitude JZ is in steady-state; a "0" if it's not. This gets set in SIXBIT and is used to flag the printed species density with a minus sign if it's in steady state. The run is terminated when all species are in steady-state; i.e., when PHOLD contains all 1's.

PROHLD(I+II,JZ) - Contains all the TERMS and all the FTERMS; used for print-out.

QOLD(M) - A holding array used in RUNKUT to hold the values of QRK for each step temporarily in case the error is too big and the step has to be repeated.

QRK(M) - One of the elements used in the Runge-Kutta solution.

R1(I) - The first species on the right-hand side of the Ith reaction.

R2(I) - The second species on the right-hand side of the Ith reaction.

R3(I) - The third species on the right-hand side of the Ith reaction.

RR1(II) - The first species on the right-hand side of the IIth photo-reaction.

RR2(II) - The second species on the right-hand side of the IIth photo-reaction.

RR3(II) - The third species on the right-hand side of the IIth photo-reaction.

SUMIN(ITCH,JZ) - The total number of atoms/cm<sup>3</sup> of type ITCH (see IATOM) at altitude JZ which were input. This is calculated in START, then used in SIXBIT to compare with SUM (the current number of atoms/cm<sup>3</sup>) and to correct the densities of all the species which contain atoms of type ITCH to force SUM to equal SUMIN.

TABO2(JZTAB) - Tabulated values of O<sub>2</sub> density, given every 2 km from 200 to 28 km. Used to get an O<sub>2</sub> profile if one is not input.

TABO3(JZTAB) - Tabulated O<sub>3</sub> densities. See TABO2.

TEMP(JZ) - The input temperature profile, in degrees Kelvin. Used as a divisor, therefore, must not contain zero values.

TERM(I) - The quantity  $K \cdot Y(L1) \cdot Y(L2) \cdot Y(L3)$  for each reaction. Each  $\frac{dY}{dt}$  is calculated as a sum of a set of TERMS. TERM(I) contains TERM for the Ith reaction; TERM(I+NREAC) also contains TERM for the Ith reaction.

TERMW(I) - Used in WEIRD, = TERM(I) calculated at  $\Delta t = H$  later than TERM. Used to calculate backwards in time to check on the error and adjust the step size.

Y(M) - The density (molecules/cm<sup>3</sup>) of species M.

YHOLD(M,JZ) - The array of Y(M) at all altitudes.

YIAST(M,JZ) - The values in YHOLD at the previous print time. Used to compare to YHOLD to see what has gone into steady-state.

YNEW(M) - The values of Y at  $\Delta t = H$ , calculated in WEIRD. Used to start the backwards calculation.

YOLD(M) - A holding array for Y used in RUNKUT. Used to restart the step if the error is too big. See QOLD.



YPRINT(M,JZ) - The same as YHOLD, except that, if a species is in steady-state, then the value is negative. This is the array that gets printed out.

YSTART(M,JZ) - The starting values of YHOLD. Used to determine if the species are in steady-state.

Y3SUN(JZ) - The  $O_2$  profile used in ZENANG to calculate the  $O_2$  scale heights (H2HOLD). This will be the same profile as in YHOLD if the solar zenith angle is less than  $90^\circ$ . If it's greater than  $90^\circ$ , then Y3SUN will have the last  $O_2$  profile before the zenith angle exceeded  $90^\circ$ .

Y4SUN(JZ) - The  $O_3$  profile used in ZENANG. See Y3SUN.

Z(JZ) - The altitudes, in kilometers, at which the calculations are being done. Highest one first. A maximum of 30 are allowed.

ZPRINT(JZ) - Same as Z except that the value is negative if all species at that altitude are in steady state. Used when printing out the species densities.

#### C. Non-Indexed Variables (Contained in COMMON /B/)

ALPHA - The solar zenith angle, in degrees, calculated in ZENANG.

EQUIL - The input criterion for deciding when a species is in steady-state.  
If  $\frac{\Delta Y}{Y \Delta t} < \text{EQUIL}$ , then the species is in steady-state.

H - The calculation step-size, in seconds, used in WEIRD and RUNKUT.

HCOUNT - A counter used to count the number of steps taken by RUNKUT or WEIRD at each altitude. Used to calculate HBAR.

IFLAG1 - Input. = 1 lets species go into steady-state; =  $\emptyset$  it does not.

IFLAG2 - Used by RUNKUT and WEIRD to know when it's time to return to the main program.

IFLAG3 - Used by ZENANG to know when it's the first time through so that starting values can be printed out.

IFLAG4 - Used to adjust the print time TPRINT.

IFLAG5 - Used to adjust TPRINT. See IFLAG4.

IFLAG6 - Used in START to tell if an  $O_2$  profile was input or if one should be constructed from TAB02.<sup>2</sup>  
 IFLAG7 - Used to tell if an  $O_3$  profile was input. See IFLAG6.  
 IFLAG8 - Input.  $\phi$  to use RUNKUT; 1 to use WEIRD.  
 IFLAG9 - Set to 1 if an error in the data is found. Run is terminated when it's = 1.  
 IJZX - = JZEND-JZMAIN. Used as part of the index for K.  
 IJ99 - = the number 99, written on magnetic tape at end of YHOLD(M,JZ) array.  
 IUNIT - The number of the tape unit where the program is to get the start-profiles. 6 $\phi$  if it's a fresh start; 13 if it's a restart.  
 IXX - Dummy index.  
 JCNTRL - Carriage control character used in one FORMAT statement in HANDLE so that the spacing on the starting values comes out right. Set in ZENANG.  
 JFLAG2 - Input.  $\phi$  for a fresh start, 1 for restart. See IUNIT.  
 JFLAG6 - Input.  $\phi$  says that fixed spacing heights are being given. If not  $\phi$ , then = the number of altitudes being given explicitly.  
 JOSHUA - Input. 1 holds the sun fixed in the sky;  $\phi$  lets the sun move naturally.  
 JZEND - The highest altitude index, equals the number of different altitudes being used.  
 JZMAIN - The altitude index of the main altitude loop in SIXBIT. Used by several subroutines.  
 LAT - The latitude, in degrees, of the place to do the calculations for.  
 LONG (The longitude, in degrees, of the place to do the calculations for. (NOT used).  
 IXL - first specie on the left side of the reaction.  
 NFREAC - The number of photoreactions input.  
 NREAC - The number of regular reactions input.  
 NSPEC - The number of species input, including #1 and #2. Actually the highest numbered species input.  
 PI - 3.14159.  
 RXL - first specie on the right side of the reaction.

T - Input initially. The time, in seconds, for which calculations have been done. Normally input as zero. Normally of no concern unless the reaction set is of interest on a time scale of less than a second, in which case T is the only thing that will keep track of the calculation time.

TDAY - Input. The number of the day. Changed as T increases and is printed out.

THOUR - Input. The hour of the day. See TDAY.

TMAX1 - Input. The maximum value which TPRINT is allowed to have during non-twilight conditions.

TMAX2 - Input. The maximum value which TPRINT is allowed to have during twilight conditions.

TMIN - Input. The minute of the hour. See TDAY.

TMONTH - Input. The month of the year. See TDAY.

TOLD - The value that T had at last print-out.

TPRINT - Input. The time between print-outs. This gets increased by  $X10$  periodically if the smallest average step-size is within a factor of  $10^3$  of TPRINT, up to a maximum of TMAX1 or TMAX2.

TQUIT - Input. Quitting time in seconds. The program will terminate when  $T = TQUIT$ .

TSEC - Input. The second of the minute. See TDAY.

ZBOTUM - Input if  $JFLAG6 = \emptyset$ . The lowest altitude to be used, in km.

ZSTEP - Input if  $JFLAG6 = \emptyset$ . The altitude interval to be used, in km.

ZTOP - Input if  $JFLAG6 = \emptyset$ . The highest altitude to be used, in km.

### 3.2 How SIXBIT Sets Up the Differential Equations

A reaction set is read in numerical form, for example

<u>Reaction No.</u>	<u>Reaction</u>	<u>Rate Coefficient Terms</u>
1	$\phi_3 \phi_4 \phi_1 \phi_5 \phi_6 \phi_1$	$1.\phi E-1\phi \quad 1.\phi E\phi \quad \phi.\phi \quad \phi.\phi$
2	$\phi_5 \phi_6 \phi_1 \phi_3 \phi_4 \phi_1$	$1.\phi E-15 \quad 1.\phi E\phi \quad \phi.\phi \quad \phi.\phi$
3	etc.	

For reaction #1, the first species number on the left-hand side ( $\phi_3$ ) is L1(1), the second ( $\phi_4$ ) is L2(1), the third ( $\phi_1$ ) is L3(1), the first species number on the right ( $\phi_5$ ) is R1(1), the second ( $\phi_6$ ) is R2(1), and the third ( $\phi_1$ ) is R3(1). The total number of reactions read in is NREAC, and the highest species number is NSPEC. Having read in the reactions, the program then determines which reactions affect each species, and whether or not each reaction is a destroyer or a producer of that species. This is accomplished by building a long one-dimensional array of reaction numbers. The first NREAC locations are for species #3, the second NREAC locations are for species #4, etc. If a reaction is a destroyer of the species, then the reaction number itself is entered in the table. If the reaction is a producer, then the reaction number + NREAC is entered. The table of reaction numbers is called NASRAS (Number and Sign of the Reactions Affecting the Species). If the reaction set consisted of the first two reactions in the example given above, then NASRAS would be set up as

#### Location

- 1) Allocated to species #3. Length 2, because there are
- 2) 2 reactions in the set
- 3) Allocated to species #4
- 4)
- 5) Species #5
- 6)
- 7) Species #6
- 8)

and would be filled as follows:

<u>Location</u>	<u>Contents</u>	<u>Explanation</u>
1	1	Reaction #1 is a destroyer of species #1.
2	4	Reaction #2 is a producer of species #1 and has had NREAC(=2) added to it.
3	1	
4	4	
5	3	
6	2	
7	3	
8	2	

The number of reaction numbers entered for each species is counted by NTERM which is indexed by the species number. In the example just given, NTERM(3) = NTERM(4) = NTERM(5) = NTERM(6) = 2, since there have been 2 reaction numbers entered for each species.

Given the arrays NASRAS and NTERM, the differential equation for each species can be formed as

$$\frac{dY}{dt} = \sum_i \text{TERM}_i$$

where  $i$  takes on all reaction numbers found in NASRAS,  $\text{TERM} = K_i Y_{L1_i} Y_{L2_i} Y_{L3_i}$  and TERM is taken positive or negative depending on whether the reaction is a producer or destroyer of  $Y$ .

In this way, SIXBIT reads the reactions and sets up the differential equations. Since the TERMS must be recalculated every step during the solution of the equation, the only things that exist permanently in the program are the reactions, NASRAS, and the current values of the species densities.

### 3.3 How SIXBIT Handles Sunlight and Photochemistry

One of the inputs to SIXBIT is latitude (LAT), longitude (LONG), date and time (TMONTH, TDAY, THOUR, TMIN, TSEC). The declination of the sun is calculated from

$$\text{DEC} = 23.445 * \text{SINF}((2.0 * \text{PI} * (30.4 * \text{TMONTH} + \text{TDAY} - 112.0)) / 365.0)$$

which is just a sine fit to the variation of the declination of the sun over a year, with the approximation that all months have 30.4 days.

The hour angle of the sun is calculated as

$$\text{TZEN} = 15.0 * \text{ABSF}(\text{FLOAT}(\text{TSEC} + 60 * (\text{TMIN} + 60 * \text{THOUR})) - 43200) / 3600$$

and the zenith angle is then calculated as

$$\text{ALPHA} = (1/\text{RAD}) * \text{ACOSF}(\text{SINF}(\text{LAT} * \text{RAD}) * \text{SINF}(\text{DEC} * \text{RAD}) + \text{COSF}(\text{LAT} * \text{RAD}) * \text{COSF}(\text{DEC} * \text{RAD}) * \text{COSF}(\text{TZEN} * \text{RAD}))$$

Once the program has ALPHA, it calculates the solar spectrum for the altitude where it's doing the calculations. To do this, the program carries the solar spectrum at the top of the atmosphere. This is carried as  $\text{FLXINF}(\text{LAMDA})$ , where  $\text{FLXINF}$  (Flux at infinity) is the flux in photons/cm<sup>2</sup>-sec-100Å and  $\text{LAMDA}$  is the wavelength index. The spectrum goes from 0 to 12,000Å in 100Å steps, so  $\text{LAMDA}$  goes from 1 to 120.

<u>Wavelength Region</u>	<u>LAMDA</u>
0-100 Å	1
100-200 Å	2
200-300 Å	3
. . . .	. .
11,900-12,000 Å	120

The solar spectrum is shown in figure 2.

The solar spectrum at the altitude of interest is calculated as

$$\phi(\lambda) = \phi_{\infty}(\lambda) \exp \left\{ - \sigma_{O_2}(\lambda)[O_2]H_{O_2}F_{O_2} - \sigma_{O_3}(\lambda)[O_3]H_{O_3}F_{O_3} \right\}$$

where  $\sigma_{O_2}(\lambda)$  is the absorption cross-section of  $O_2$  as a function of wavelength,  $\sigma_{O_3}(\lambda)$  is the absorption cross-section of  $O_3$ ,  $[O_2]$  and  $[O_3]$  are the  $O_2$  and  $O_3$  concentrations,  $H_{O_2}$  and  $H_{O_3}$  are the  $O_2$  and  $O_3$  scale heights at the altitude of interest, and  $F_{O_2}$  and  $F_{O_3}$  are factors which play the same role that  $\sec \alpha$  would in a plane-parallel atmosphere.  $\sigma_{O_2}(\lambda)$  and  $\sigma_{O_3}(\lambda)$  are carried by the program. The values used are shown in figures 3 and 4.  $[O_2]$  and  $[O_3]$  are the densities calculated at each point in time by the program, except that, when the sun goes down below the horizon, the  $O_2$  and  $O_3$  profiles at  $90^\circ$  are held and used until the sun comes back up to  $90^\circ$  again. The physical justification for this is that, for  $\alpha > 90^\circ$ , the absorption is controlled primarily by the density at the point of closest approach to the earth of the sun's rays, which is the point at which  $\alpha = 90^\circ$ .

$H_{O_2}$  and  $H_{O_3}$  are calculated from the existing profiles of  $O_2$  and  $O_3$ .  $F_{O_2}$  and  $F_{O_3}$  are determined from equations given by Swider [1964].

The flux at a given altitude is determined entirely from absorption coefficients carried by the program. The photo-production (or loss) rates of particular species are determined from the calculated fluxes and from absorption coefficients which must be read into the program. Absorption coefficients, like the flux values, are handled in 100-Å bands. Values must therefore be entered so that the average over the 100-Å band is correct.

A special case exists for  $Ly\alpha$  ( $\lambda_{L\alpha} = 13$ ). Since most of the energy is at 1215Å, the cross section of  $O_2$  suitable to 1215Å is used in the cross-section value.

All the photo calculations are repeated every print-out time, so print-out times must be controlled so that the change in solar zenith angle is not excessive. (See TMAX1 and TMAX2 in the input data.)

Solar spectra at a variety of altitudes, calculated by SIXBIT, are shown in Figures 5, 6, 7, and 8.



### 3.4 Methods of Solution of the Time-Dependent Differential Equations

There are two methods of solution within SIXBIT, with selection made via a 0/1 flag in the input data. 0 is a Runge-Kutta solution; 1 is a partial integration technique. In general the partial integration technique works best if the rapidly changing species are minor species which are imbedded in a relatively stable sea of major species (which covers most atmospheric problems) - Runge-Kutta would be best for the simple 2-reaction set we have been using as an example.

#### A. The Runge-Kutta Routine, RUNKUT

This has been taken with no changes from Romanelli [1964].

#### B. The Partial Integration Routine, WEIRD

The equation for any species can be written as

$$\frac{dY_m}{dt} = \sum_{i \neq m} K_i Y_{1i} Y_{2i} Y_{3i} - Y_m \sum_{j \neq m} K_j Y_{1j} Y_{2j}$$

which says that  $Y_m$  can be factored out of every loss term and never appears in the gain terms. (This is an approximation if species  $m$  appears twice or more on the left-hand side of a reaction and not at all on the right-hand side.) Now rewrite this as

$$\frac{dY_m}{dt} = f_m - g_m Y_m$$

where  $f_m$  and  $g_m$  can be functions of all the  $Y$ 's except  $Y_m$ .

Now, taking  $f_m$  and  $g_m$  to be constant over a step in time, this can be integrated directly to give

$$Y_m(H) = \left\{ Y_m(0) - \frac{f_m}{g_m} \right\} e^{-g_m H} + \frac{f_m}{g_m}$$

where  $f_m$  and  $g_m$  are evaluated at  $t=0$ . The accuracy of a step is checked by starting with  $Y_m(H)$  and calculating backwards in time ( $t=H$ ) to get  $Y_m^B(0)$ , which should be the same as  $Y_m(0)$ . Agreement to 1 part in  $10^3$  is satisfactory here in most cases. If the agreement is not this good, the step-size is halved and the calculation repeated. If the agreement is satisfactory, then the step forward is recalculated using the average  $f$  and  $g$  over the interval.

Any typical method for solving differential equations (such as Runge-Kutta) makes two approximations; that most quantities stay constant over a step and that the integral can be approximated by a Taylor's series. The partial integration method merely recognizes that there is no reason to approximate the integral since it can be evaluated as it stands.

## 3.5 Through the Program in Detail

In this section we will go through the program in the logical (working) order, with special attention to areas which may have to be changed to run on other machines.

There are no separate dimension statements. All dimensioned variables are in COMMON/A/, which is carried by the main program and all the sub-routines. COMMON/B/ carries all the non-indexed variables needed in more than 1 subroutine. Type statements (REAL and INTEGER) have been used to allow more reasonable variable names.

The comment cards carry enough information to get the data in properly.

READ (13,997) ICRUD - This is a dummy read which just insures that the program will always read from unit 13 (which holds the profiles for restart purposes) before it writes on 13. This is necessary on our system to avoid changing control cards between runs.

CALL REACTS - Subroutine REACTS reads in the reactions, counts the reactions and the species numbers, and reads and counts the photoreactions. The following describes REACTS.

DO 10 I1=1,51

. . .

10 CONTINUE - This loop reads in the reactions until it finds a 99 in columns 1 and 2, at which point it jumps to statement 20. If it does not find a 99 in the first 51 reactions, it will print an error message, set IFLAG9 = 1, return to the main program, and terminate. This loop also searches out the largest species number existing in the reactions.

20 NREAC = I1-1 - The number of reactions is I1-1 since it was on I1 when it found the 99, and that is not a reaction.

NSPEC = NSPEC-2 - This gets the actual number of species input, not the highest numbered species. (This assumes that you have used all the numbers between 3 and NSPEC. If NSPEC = 10 but 5 is never used as a species number, no harm is done, but the program thinks 5 is a real species.)

DO 30 I2=1.21

...

30 CONTINUE - This reads in the photoreactions; same game as the regular reactions.

RETURN to SIXBIT

CALL HEIGHTS - This is a trivial subroutine which sets up the altitudes.

IF(JFLAG6.EQ.0) GO TO 100 - JFLAG6=0 says that you have given the program the highest altitude, the lowest altitude, and the step size (in kilometers). JFLAG6≠0 says you have given it JFLAG6 altitudes, the highest one first.

RETURN to SIXBIT

CALL ALGEBRA - ALGEBRA calculates the rate coefficient array K and sets up the arrays NASRAS, NUSRUS, NTERM, and NTERM.

DO 20 I2=1,NREAC

...

20 CONTINUE - This loop sets up NASRAS and NTERM. The first part, down to statement 200, just eliminates species which appear on both sides of the reaction.

RETURN to SIXBIT

CALL START - This does most of the initializing needed.

The first DATA statement contains the three arrays of constants needed by RUNKUT (ARK, BRK, and CRK) and initializes several arrays. HBAR is set to 1 since WEIRD uses HBAR to get a beginning step-size. The first two species in YHOLD are set to 1, since these are the unit density species that the program uses.

The second and third DATA statements contain FLXINF, the solar photon flux at infinity in photons/cm<sup>2</sup>-sec-100Å, starting with the 0-100Å band (LAMDA = 1).

The fourth and fifth DATA statements contain KABSN2, the absorption coefficient for N<sub>2</sub> in cm<sup>2</sup>, starting with the value for the 0-100Å band. This absorption coefficient is not used at present. If you ever want to do F-region calculations, UV absorption by N<sub>2</sub> may become important.

The sixth and seventh DATA statements contain KABS03, the absorption coefficient for O<sub>3</sub> in cm<sup>2</sup>.

The eighth and ninth contain KABS02, the absorption coefficient for O<sub>2</sub> in cm<sup>2</sup>.

The tenth contains TAB02, the tabulated O<sub>2</sub> densities in molecules/cm<sup>3</sup>, given from 200 km to 28 km in 2 km steps.

The eleventh DATA statement contains TAB03, the tabulated O<sub>3</sub> densities, just like TAB02.

DO 10 M1=3,NSPEC

...

10 CONTINUE - reads in species numbers and the number of atoms/molecule of the different types. Note that one card must be present for every species, but that they do not have to be in order.

READ (60,994) ...

READ (60,993) ... - the latitude and calendar information gets read in here even though it is not needed until subroutine ZENANG. This is done so that the starting concentration profiles, which do get read in START, can be the last cards in the data deck. By having the data arranged in this way, JFLAG2 can be set to pick up the starting profiles from cards or magnetic tape without having to rearrange the data deck.

DO 2Ø M3=2,NSPEC

. . .

2Ø CONTINUE - This loop reads in the starting profiles. It keeps reading until it finds a "99" for a species number, so the loop is set to go from 2 to NSPEC. This way, even if you give it a profile for every species, it will try to read one more and thus find the "99". Each time it reads a species number, it looks to see if that species is #3 or #4 ( $O_2$  or  $O_3$ ). That way, if  $O_2$  and/or  $O_3$  profiles are not input, it can generate its own from TAB02 and/or TAB03, since it has to have  $O_2$  and  $O_3$  profiles to do the sunlight calculations. It also set  $Y_{NEW}(M_4) = 2.Ø$  for each species for which it has profiles, so that any species not specified can be given a profile later of  $5 \times 10^{-6}$  times the  $O_2$  profile. This is just to avoid having zeroes for profiles, since the solutions are often quite slow when they have to work with true zeroes rather than just small numbers.

PRINT 996

IFLAG9=1

GO TO 9000 - if the previous loop never found a "99" to indicate the end of the profiles, it will print an error message, return to SIXBIT, and terminate the run.

3Ø IF(IUNIT.EQ.13)REWIND 13 - if the loop found a "99", it will come here and rewind tape unit 13 if it read 13 to get the profiles. IF(IFLAG6.EQ.1 etc. - if both  $O_2$  and  $O_3$  profiles were input, it's happy and will go to 4Ø. If the  $O_2$  and/or  $O_3$  profiles were not input, then IF(Z(1).LE.200.0 etc. - the altitude range must lie within 30-200 km or else the program cannot construct  $O_2$  and/or  $O_3$  profiles internally. If it is not, it will terminate.

4Ø DO 5Ø JZ3=1,JZEND

. . .

5Ø CONTINUE - This loop sets up the  $O_2$  profiles to be used for the sunlight calculations (Y3SUN) from the tabulated values,

regardless of whether or not a profile was input. If the calculations are being started in daytime, then this profile will be replaced after the first step by the calculated profile. If the calculations are being started at night, then this avoids having the sunrise period being controlled by a nighttime profile. I2 and I1 are the index values of the TABO2 values which are at altitudes that are required for the calculations. This loop also puts the O<sub>2</sub> profile derived from TABO2 into YHOLD if an O<sub>2</sub> profile was not input (i.e., if IFLAG7 = 0).

DO 70 JZ4=1,JZEND

...

70 CONTINUE - This does the same thing for the O<sub>3</sub> profiles that the previous loop did for the O<sub>2</sub> profiles.

80 DO 85 M6=5,NSPEC

...

85 CONTINUE - This loop makes use of the flag values contained in TNEW (set in the "DO 20" read loop) to put in profile =  $5 \times 10^{-6}$  times the O<sub>2</sub> profile if the profile was not input.

DO 110 ITCH=1,10

...

110 CONTINUE - This loop calculates the total number of atoms/cm<sup>3</sup> of each different type in the input data. CHECK is used to find out how many different types of atoms have been declared. ITCHXX is set to the total number of different types of atoms (actually to the first value of ITCH which is followed by CHECK < 1.0).

...

RETURN TO SIXBIT

Everything down to this point will be passed through by the program once per run. The statements after this are in a big loop which will be passed through many times.

1 $\emptyset$  CALL ZENANG - This subroutine calculates the zenith angle of the sun (ALPHA), prints out the starting values that were input, and calculates the scale heights of O<sub>2</sub> and O<sub>3</sub> for all the altitudes.

IF(IFLAG3.NE. $\emptyset$ ) GO TO 1 $\emptyset$  - IFLAG3 was set to zero in the first DATA statement in START. The first time through ZENANG, ALPHA is calculated, the starting values are printed out, and IFLAG3 is set to 1. The rest of the time, since IFLAG3 is not = 0, printing the starting values is omitted, and the calculation of ALPHA is skipped if the sun is being held fixed in the sky.

DEC = . . . - This calculates the declination of the sun in degrees. This equation is a sine fit to the annual variation of the solar declination, and carries the approximation that every month has 30.4 days.

PRINT 998 - This puts the "STARTING VALUES" label on the print-out.

JCNTRL =  $\emptyset$  - This is a carriage control character that will keep the print-out from skipping to the top of the next page, so that the "STARTING VALUES" label will be in the proper place.

THOLD = TPRINT

TPRINT =  $\emptyset$  - This will keep time from being advanced by the print-out routine as is normally done.

THOLD will let TPRINT be recovered after the print-out.

TZEN = . . . - This calculates the hour angle of the sun, which is measured in degrees (1 hour = 15 degrees) relative to noon.

ALPHA = . . . - This calculates the zenith angle of the sun, in degrees away from vertical.

CALL HANDLE - This is the subroutine that does all the print-out.

TX = . . .

. . .



TSEC = TX - This section adds TPRINT onto the previous calendar time to get the new calendar time. Note that TX, TDAY, THOUR, TMIN, TSEC are all integers by virtue of the type statement.

ITSEC = TSEC + 100

. . .

ITDAY = TDAY + 100 - on the CDC 3800, an I format which is too small drops digits from the left. Therefore, 104 printed in an I2 format comes out an 04. This lets 8 AM on June 1 be printed out as 06/01 08/00/00 rather than as \_6/\_1 \_8/\_0/\_0.

ITIME = KLOCK(1)

TIME = ITIME/1000 - KLOCK is a system subroutine that reads a clock in the CDC 3800 in milliseconds, relative to the start of the program.

The rest of this subroutine is a straightforward print-out of the reaction terms, the species densities, the major destruction reactions, and the major production reactions.

Right after statement #40 (CONTINUE) is IF(JCNTRL.EQ.0) GO TO 9000. Since the major destruction and production reactions are not determined until after the calculation has been advanced through a step, their print-out is skipped the first time through. (Note that JCNTRL is used as a carriage control character in FORMAT 999, used in the first print statement.)

RETURN to ZENANG

JCNTRL = 1 - This carriage control character is now set to 1 and will stay that way throughout the rest of the run.

TPRINT = THOLD - The true value of TPRINT is recovered.

GO TO 100 - This will skip by the section which starts with statement #10. This section, reached by the first statement in the program (IF IFLAG3 . . .) is just the calculation of ALPHA without all the extra statements required the first time through.

100 IF(ALPHA.GT.90.0+SQRTF(Z(1))) GO TO 9000 - The equation  
 $\alpha_s = 90 + \sqrt{Z_s}$ , where  $\alpha_s$  is the zenith angle of the sun in degrees  
 and  $Z_s$  is the height of the shadow of the solid earth in kilometers,  
 is a useful approximation. This statement says to skip all the  
 calculations about solar fluxes if the height of the shadow is above  
 the highest altitude of interest.

IF(ALPHA.GT.90.0) GO TO 300 - if  $\alpha < 90^\circ$ , the following loop will  
 take the  $O_2$  and  $O_3$  profiles to be used for the solar flux attenuation  
 calculations (Y3SUN and Y4SUN) as the current calculated profiles (YHOLD).  
 If  $\alpha > 90^\circ$ , it wants to use the profiles that existed at  $90^\circ$  (or the  
 closest it got to  $90^\circ$ ), so it skips the replacement loop.

DO 200 JZ1=1JZEND

...

200 CONTINUE - This just puts the  $O_2$  and  $O_3$  profile into Y3SUN and Y4SUN.

The rest of ZENANG calculates the scale heights of  $O_2$  and  $O_3$  at the  
 altitudes of interest, since this is what PRODUC needs to calculate  
 the attenuation of the solar photon flux. It does this by fitting  
 the top two points in each profile with an exponential, and deter-  
 mining from this the total amounts of  $O_2$  and  $O_3$  that lie above the  
 top altitude. At each altitude, it then determines the total amount  
 of  $O_2$  and  $O_3$  from there to the top by doing a simple sum, adds on  
 the amount determined to lie above the top altitude, and then deter-  
 mines what the scale heights have to be at that point for the inte-  
 grated densities above that point to come out right.

The exponential form is

$$Y(Z_1) = Y(Z_2) e^{-(Z_1-Z_2)/H}$$

so that, if  $Z_1$  is the top altitude and  $Z_2$  is the next-to-the-top, then

$$H = (Z_2 - Z_1) / \ln(Y(Z_1)/Y(Z_2)) \quad .$$

The total number of molecules/cm<sup>2</sup> above  $Z_1$  is

$$X = \int_{Z=Z_1}^{Z=\infty} Y(Z_1) e^{-(Z - Z_1)/H} dz$$

which gives

$$X = HY(Z_1) \quad .$$

Now back to the program.

```

300 IF(Y3SUN(2).GT.Y3SUN(1)) GO TO 310 - If the top two points on the
    profile indicate that the density is increasing with altitude, then
    the exponential extrapolation of the profile to infinity will give
    an infinite number of molecules. Therefore, if the density is in-
    creasing, the program will print out a message (PRINT 997), set
    IFLAG = 1, return to SIXBIT, and terminate. If the density is de-
    creasing, it goes to statement 310.

310 IF(Y3SUN(1).GT.0.0) GO TO 320 - This avoids a division by zero in
    determining the scale height for O2. If the top O2 density is zero,
    then
    H2HOLD = 1.0 - The scale height is taken as 1 and it jumps to 330.
    Otherwise it goes to

320 H2HOLD(1) = (Z(2)-Z(1))/LOGF(Y3SUN(1)/Y3SUN(2)) which is just the
    equation for the scale height given earlier.

330 IF(Y4SUN(2).GT.Y4SUN(1)) GO TO 340.

350 H3HOLD(1) = . . . - This is the same as the preceding block, except
    for O3 instead of O2.

400 ADD3 = Y3SUN(1)*H2HOLD(1)
    ADD4 = Y4SUN(1)*H3HOLD(1) - ADD3 and ADD4 are the integrated den-
    sities of O2 and O3. These statements, using the equation for X
    given before, initialize the sums.

DO 410 JZ2=2,JZEND - This starts the integration.

```

ADD3=ADD3+(Y3SUN(JZ2-1)+Y3SUN(JZ2))\*(Z(JZ2-1)-Z(JZ2))/2.0

ADD4 = . . . - These take the total numbers of molecules/cm<sup>2</sup> between two altitudes as the linear average of the end-points times the distance between the two altitudes, and adds them onto the sum.

H2HOLD(JZ2)=ADD3/Y3SUN(JZ2)

H3HOLD(JZ2) = . . . - This uses the equation  $X = HY(Z_1)$  to determine the effective scale height at JZ2.

410 CONTINUE

RETURN to SIXBIT

DO 100 JZMAIN=1,JZEND - Here begins the calculation proper. JZMAIN is in COMMON/B/ and will be used in several places to know what altitude is being treated.

IJZX = JZEND - JZMAIN - This is part of a compound index that will be needed in RUNKUT or WEIRD.

DO 30 ML=1,NSPEC

. . .

30 CONTINUE - This transfers the species densities at this altitude to a singly-dimensioned array, since it is faster to use a single index than to use a double index.

CALL PRODUC - This is the subroutine that uses the scale heights calculated in ZENANG to determine the solar flux at Z(JZMAIN), and then determines the FTERM's for the photoreactions from this flux.

CALL Q9EXUN - This is a system subroutine which suspends the underflow detection, and simply replaces an underflow (a number less than  $\sim 10^{-308}$ ) by zero without writing an error message.

IF(NFREAC.EQ.0) GO TO 9000 - If there are no photoreactions, this subroutine will be skipped.

ALPHAR=ALPHA\*PI/180.0 - ALPHAR is ALPHA in radians.

REARTH = 6371.0 - The radius of the earth in kilometers.

IF(ALPHA.GT.90.0) GO TO 1000 - This statement and statement 1000 divide the calculations into 3 regions;  $\alpha < 90^\circ$ ,  $90 < \alpha < 90 + \sqrt{Z}$ , and  $\alpha > 90 + \sqrt{Z}$ . For  $\alpha < 90^\circ$ , the calculation of F02 and F03 is done using equation 53 in Swider [1964]. For  $90 < \alpha < 90 + \sqrt{Z}$ , F02 and F03 are calculated with equation 47 in Swider. If  $\alpha > 90 + \sqrt{Z}$ , the photo terms are set to zero with the loop at statement 1000. F02 and F03 can be thought of as  $\sec \alpha$  modified for the curvature of the earth.

Having calculated F02 and F03 for either  $\alpha < 90^\circ$  or  $90 < \alpha < 90 + \sqrt{Z}$ , you wind up at

3000 DO 310 LAMDA=1,120

...

310 CONTINUE - This loop calculates the solar photon flux as a function of wavelength, FLUX(LAMDA), using the flux at infinity (FLXINF), which was given in a DATA statement in START, the absorption coefficients for  $O_2$  and  $O_3$  (KABS02 and KABS03) which were given in DATA statements in START, the  $O_2$  and  $O_3$  densities (Y3SUN & Y4SUN) which were set up in ZENANG, and F02 and F03 which were just calculated.

DO 330 II=1,NFREAC

...

330 CONTINUE - The rate that a photoreaction of the form  $A + h\nu \rightarrow B + C$  goes is

$$\frac{dA}{dt} = [A] \int_0^{\infty} \sigma(\lambda) \phi(\lambda) d\lambda$$

In SIXBIT, the integral is called FRATE. This loop just calculates FRATE.

GO TO 9000

9000 CALL R9EXUN - This restores the system underflow detection.

RETURN to SIXBIT

HCOUNT = 0 - This is a counter that will be used later.

IF(IFLAG3.EQ.1) GO TO 40 - IFLAG3 is the input flag (0 or 1) that picks the method of solution, either RUNKUT (the Runge-Kutta solution) or WEIRD (the partial integration solution).

RUNKUT:

CALL Q9EXUN - This suspends underflow detection, as in ZENANG.

H=HBAR(JZMAIN)\*3.0 - HBAR was set to 1.0 in START. Later HBAR will be the average step-size over the previous print interval. This statement assumes that the biggest allowable step is probably bigger than the previous average. H is the step to be used in the calculation.

10 TCHECK = T-TOLD+H

...

IFLAG2 = 1 - If a step of size H will put the time beyond the time for the next print-out, then H is reduced to get time just to the print time, and IFLAG2 is set to 1. This will return the program to SIXBIT at the end of the step.

20 DO 30 M1=2, NSPEC

...

30 CONTINUE - This holds onto the current values of Y and QRK in case the error is too big in the next step and the calculation must be repeated.

40 DO 90 JRK=1,4 - This starts the 4 calculations involved in a fourth-order Runge-Kutta solution.

DO 50 I1=1,NREAC

...

50 CONTINUE - This calculates the TERM for each reaction (see section 2).  
DO 52 IT1=1,NFREAC

...

52 CONTINUE - This calculates the FTERM's for the photoreactions.

JRKX = (JRK-1)\*NSPEC - Part of a compound index to be used later for KRK.

DO 7 $\phi$  M2=3,NSPEC - This starts the loop that calculates the time derivatives for the species.

MJRK = JRKX+M2 - The rest of the compound index to be used later for KRK.

IIIX=(M2-3)\*NREAC - Part of a compound index to be used for NASRAS.

DY= $\phi$ . $\phi$  - DY is the time derivative for species M2. It will be transferred to an indexed variable after all the TERM's have been added on.

NNSTOP=NTERM(M2) - This is the number of TERM's in NASRAS which affect species M2. This statement is made because NTERM has to be the end of a DO loop specification, and indexed variables cannot be used for that.

DO 6 $\phi$  NN=1,NNSTOP - This begins the loop to pick the TERM's for M2 out of NASRAS and add them onto DY.

IF(NASRAS(IIIX+NN).LE.NREAC) GO TO 55 - This picks a reaction number from NASRAS and decides if it is a production reaction or a destruction reaction. If it is >NREAC, it is a production reaction, and it goes to

DY=DY+TERM(NASRAS(IIIX+NN)), which adds the TERM for that reaction to DY. If the reaction number is  $\leq$ NREAC, it goes to

55 DY=DY-TERM(NASRAS(IIIX+NN)). Either way, it winds up at

6 $\phi$  CONTINUE, which sends it back to get the next reaction number from NASRAS.

IIIX=(M2-3)\*NFREAC

. . .

65 CONTINUE - This section is just like the one before, except that this one picks the FTERM's from NUSRUS (the photoreactions) and adds them to (or subtracts them from) DY.

KRK(MJRK)=DY - This just puts DY into an indexed array.

7 $\phi$  CONTINUE - This is the end of the M2 loop.

Now that it has all the time derivatives, it does the loop

DO 8 $\phi$  M3=3, NSPEC

. . .

8 $\phi$  CONTINUE - which calculates Y at one of four places in the interval H in a standard Runge-Kutta method.

9 $\phi$  CONTINUE is the end of the Runge-Kutta loop begun at statement #4 $\phi$ .  
K5MAX =  $\phi$ . $\phi$ .1

. . .

10 $\phi$  CONTINUE - This determines the maximum value (K5MAX) of a ratio of differences of the KRK's, which is a measure of the error. If K5MAX <  $\phi$ .1, the step had too big an error and it should be repeated with a smaller step.

IF(K5MAX.IT. $\phi$ .1) GO TO 12 $\phi$  - If the error is too big, it cuts the step-size down with

H=H\* $\phi$ . $\phi$ 8/K5MAX. It sets

IFLAG2= $\phi$ , uses

DO 11 $\phi$  M5=2, NSPEC

. . .

11 $\phi$  CONTINUE to recover the starting values, and goes back to statement #4 $\phi$  to redo the step. If the error was small enough, it winds up at

12 $\phi$  T=T+H which advances the time

H=H\* $\phi$ . $\phi$ 8/K5MAX which gets a value for the next step

HCOUNT=HCOUNT+1 - which is a counter on the number of steps it's taken (this was zeroed in SIXBIT), and uses

IF(IFLAG2.EQ. $\phi$ ) GO TO 1 $\phi$  to see if it is time to return to SIXBIT or not.

CALL RETURN - Restores the system underflow.

WEIRD

Section 3.4 B gives the general approach used here.

AKRACY=1. $\phi$ E-3 - This is the largest allowed difference between the starting value of the species density (Y) and the value back-calculated from T+H (YBACK).



```

HMIN=1.0E-6 - is the minimum allowable step-size. H will never
be allowed to get smaller than this regardless of the accuracy
requirement.
YNEW(1)=1.0 - This will be needed later.
CALL Q9EXUN - Suspends system underflow detection (see ZENANG
or RUNKUT).
H=HBAR(JZMAIN)*3.0 - as in RUNKUT
IF(H.LT.TPRINT). . .
. . .
IFLAG2=1 - as in RUNKUT
10 DO 100 I1=1,NREAC
. . .
200 CONTINUE - Calculation of TERM's and FTERM's as in RUNKUT.
DO 500 M1=3,NSPEC
. . .
500 CONTINUE - This calculates the quantities F and G. This is the same
as the calculation of DY in RUNKUT, except that all gain terms are
added to F, all loss terms are added to G, and Y is factored out
of G.
600 DO 700 M2=3,NSPEC
. . .
700 CONTINUE - This loop calculates the values of Y(YNEW) with a time
step H. The equation used is that given in Section 3.4 B, with
sub-cases for F and/or YG being effectively zero.
DO 800 I2=1,NREAC
. . .
1200 CONTINUE - This section calculates the new TERM's (TERMW), the
new phototerms (FTERMW), and the new F's and G's at the point T+H,
just as the first part of this subroutine calculated TERM's, FTERM's,
F's and G's at the point T.
DELMAX = 0.0
. . .

```

1400 CONTINUE - This section calculates backwards in time, just as before except with a step-size -H, gets the new values of Y at time T+H-H (YBACK), determines the difference between YBACK and Y(DEL), and keeps track of the maximum value of DEL(DELMAX).  
 IF(DELMAX.LE.AKRACY) GO TO 1500 - If the maximum error (DELMAX) is bigger than AKRACY, then the step-size is checked with  
 IF(H.LT.1.01\*HMIN) GO TO 1500. If the step-size is bigger than the minimum value, then the step is decreased either by a factor of 2 or down to HMIN, whichever is larger. IFLAG2 = 0, and it returns to 600 to repeat the step with a smaller step-size. If either DELMAX < AKRACY or H ~ HMIN, then it winds up at

1500 DO 1700 M6=3, NSPEC  
 . . .

1700 CONTINUE which just repeats the step forward using the average values of F and G (FBAR and GBAR).  
 T=T+H  
 . . .

9000 CALL Q9EXUN - just as in RUNKUT except for the way the step-size is increased.  
 RETURN TO SIXBIT

Control is now returned to SIXBIT from RUNKUT or WEIRD, whichever was being used. The species densities (Y's) for the altitude Z(JZMAIN) have been advanced from T to T+TPRINT, and HCOUNT contains the number of steps that were required.

50 HBAR(JZMAIN)=TPRINT/HCOUNT - gives the average step-size used over the series of calculations.  
 IFLAG2 = 0 - reset for the next altitude.  
 DO 65 ITCH=1, ITCHXX  
 . . .

70 CONTINUE - This determines the number of atoms of each different type/cm<sup>3</sup> at this altitude according to the new set of densities, scales the densities so that the number/cm<sup>3</sup> stays constant,

scales Y(2) every time to accumulate the total amount of scaling that has occurred, and puts the densities back into YHOLD.

DO 73 I=1,NREAC

. . .

76 CONTINUE - The TERM's and FTERM's from the last step in RUNKUT or WEIRD are stored in PROHOLD. They will be printed out later.

T=TOLD - T is reset to TOLD for the calculations at the next altitude.

140 CONTINUE - Go back and take the next altitude.

Having completed the JZMAIN loop, all altitudes have been advanced from T to T+TPRINT.

T=T+TPRINT - T was reset to TOLD at the end of the JZMAIN loop, this puts it back to where it should be.

IF(IFLAG1.EQ.0) GO TO 150 - IFLAG1 was one of the input parameters. If IFLAG1= 0, then it does not make equilibrium checks. If IFLAG1=1, then it does.

DO 140 JZ1=1,JZEND

. . .

140 CONTINUE - This determines what has gone into equilibrium. A species is declared to be in equilibrium (1) if both the current species density (YHOLD) and the species density at the last print-out (YLAST) are less than  $10^{-50}$ , i.e., if it looks like it is at zero and plans to stay there, (2) if the current species density is down by  $10^5$  or more from the starting value (YSTART) and is also less than  $1.0$ , i.e., it looks like it is going to zero, (3) if the fractional change per second ( $\frac{1}{Y} \frac{\Delta Y}{\Delta t}$ ) over the last print interval is less than the value of EQUIL specified on the input data. If YHOLD(M,JZ) meets any of these criteria, then it is declared to be in equilibrium, then JPULL(JZ) is set =1 and HBAR(JZ) is set to TQUIT so that it will not interfere with a later section which adjusts TPRINT, the print-out interval.

150 DO 170 JZ2=1,JZEND

. . .

170 CONTINUE - This loop transfers YHOLD to YPRINT and Z to ZPRINT. When it transfers, it uses PHOLD to make YPRINT negative if the species is in equilibrium, and it uses JPULL to make ZPRINT negative if all the species at that altitude are in equilibrium, CALL PHYSICS - This subroutine determines which reactions are the major producers and destroyers of each species at each altitude. It gives the major producer (or destroyer) of each species, and then any other reactions which are within a factor of 10 of the major one. All the TERM's and FTERM's that PHYSICS needs are in PROHLD, but it must look at either NASRAS or NUSRUS (depending on where it is) and then decide if the reaction it has is a producer or a destroyer.

DO 800 M1=3,NSPEC - This picks a species number to look at.

IIIX=(M1-3)\*NREAC

IIFX=(M1-3)\*NFREAC - Part of compound indices that will be needed later.

NNSTOP=NTERM(M1)+NFTERM(M1) - Part of a DO-loop parameter, similar to the ones used in RUNKUT and WEIRD

NTX=NTERM(M1) - Just a renaming since this gets used quite a bit later.

DO 700 JZ1=1,JZEND - This picks a particular altitude to look at.

DO 100 ILOOK1=1,4

. . .

100 CONTINUE - This zeros the two arrays. The next section will make four passes through the reactions. The first pass will determine the biggest destroyer of species M1 at altitude JZ1 and put the reaction number in ILOSS(1), and determine the biggest producer and put that reaction number in IGAIN(1). The second pass will pick up the next biggest producers and destroyers and, if they are within a factor of ten of the biggest ones, put them into ILOSS(2) and IGAIN(2), etc.

DO 600 ILOOK2=1,4 - This starts the four passes described above.  
 ILMAX=IGMAX=0  
 TLMAX=TGMAX=0.0 - ILMAX and IGMAX are the reactions which are the  
 biggest destroyer and biggest producer of species M1. TLMAX and  
 TGMAX are the values of the TERM for ILMAX and the TERM for IGMAX.  
 DO 500 NN=1,NNSTOP - This starts the search through the TERM's  
 and FTERM's.  
 IF(NN.GT.NTX) GO TO 110 - If  $NN \leq NTX$  (which is the same as  
 $NTERM(M1)$ ) then it is looking at the regular reactions. If  $NN \geq NTX$ ,  
 it is looking at photoreactions.  
 It gets the reaction with  
 $NX=NASRAS(IILX+NN)$  or with  
 110  $NX=NUSRUS(IILX+NN-NTX)$ . In either case, they wind up at  
 150  $IILX=ILOOK2-1$  which is a parameter that will be needed later.  
 IF(NN.GT.NTX.AND.NX.GT.NFREAC) GO TO 300 - If  $NN > NTX$ , it is  
 looking at photoreactions. If  $NX > NFREAC$ , then it is looking at  
 a producer of M1. It thus goes to statement #300.  
 IF(NN.GE.NTX.AND.NX.GT.NREAC) GO TO 300 - If  $NN \leq NTX$ , it is look-  
 ing at regular reactions. If  $NX > NREAC$ , then it is looking at a  
 producer of M1. It thus goes to statement #300.  
 DO 200 ILOOK3=1,IILX  
 . . .  
 200 CONTINUE - This looks through the list of the destruction reactions  
 already found to see if this reaction has been entered previously.  
 If it has, it jumps to statement #500.  
 Otherwise it winds up at  
 250 IF(NN.GT.NTX) GO TO 260 - This statement and the nine following  
 (through the third GO TO 500) compare the TERM (or FTERM) to the  
 biggest TERM found so far (TLMAX). If this TERM (or FTERM) is  
 bigger than TLMAX, then TLMAX is set equal to this TERM, the reaction  
 number (NX) (or  $NX+NREAC$  in the case of photoreactions) is stored in  
 ILMAX, and it goes to statement #500.

300 IF(NN.GT.MTX) GO TO 310

...

500 CONTINUE - This section handles production reactions just as destruction reactions were handled in the preceding section. The biggest TERM is stored in TGMAX, and the reaction number is IGMAX.

IF(ILOOK2.EQ.1) GO TO 550 - If this is the first time through, it goes to

550 ILOSS(1)=ILMAX

...

BIGG=TGMAX - Which puts ILMAX into ILOSS(1), IGMAX into IGAIN(1), and holds the TERM values in BIG2 and BIGG for later use. If ILOOK2 is greater than 1, it does

IF(TLMAX.GE.0.1\*BIG2) . . .

...

GO TO 600 - Which enters those reactions into the appropriate ILOSS and IGAIN only if they are within X10 of the maximum values. Having finished the ILOOK2 loop, it goes to

IF(ILOSS(1).EQ.0) GO TO 610 - If ILOSS(1)=0, then there were no loss processes for M1, and -1 will be entered into the final arrays with statement #610. Otherwise, the final arrays (ILOSSA, ILOSSB, ILOSSC, and ILOSSD) are filled with the values of ILOSS+100, which gives leading zeroes as in HANDLE.

620 IF(IGAIN(1).EQ.0) . . .

...

630 . . . - Same as above for the gain processes.

700 CONTINUE - Return to get another altitude.

800 CONTINUE - Return to get another species.

RETURN TO SIXBIT

CALL HANDLE - This subroutine, which prints out the TERM's and FTERM's the species densities, and the major production and loss reactions determined in PHYSICS, was discussed earlier.

IF(JJFLAG.NE.1) GO TO 175 - JJFLAG was input as 0 or 1. If it was 0, the next statement is skipped. If it was 1, it goes through

CALL MICROPLT - This subroutine generates microfilm plots of the species densities. Samples are given in Appendix D. No details of the workings of this subroutine will be given. Anyone not working on the Boulder CDC 3800 will have to delete this subroutine and the call to it. For people using the CDC 3800, note that the name and extension in the first DATA statement must be changed so that we do not get your microfilm.

175 RETURN TO SIXBIT  
TOLD=T - TOLD is advanced in preparation for the next set of calculations.

IF(TOLD.GE.TQUIT) GO TO 8 $\phi\phi$  - TQUIT was the time to quit which was input. If  $T < TQUIT$ , it goes to the next section, which increases the print interval (TPRINT).

This section works well only if T was input as  $\phi.\phi$  initially. In normal operation, the result of this section is to have the print-outs come at  $T=1, 2, 3, \dots, 9, 1\phi, 2\phi, 3\phi, \dots, 9\phi, 1\phi\phi, 2\phi\phi, 3\phi\phi, \dots, 9\phi\phi, 1\phi\phi\phi, 2\phi\phi\phi$ , etc., which keeps you from being buried in paper while still giving regions of rapid change in sufficient detail to see what is going on.

IFLAG<sup>4</sup>=IFLAG<sup>4</sup>+1 - IFLAG<sup>4</sup> is a counter which is treated as the second significant digit of T. (This is true if T starts at  $\phi.\phi$  and if TPRINT is  $1 \times 10^n$ .)

IF(IFLAG<sup>4</sup>.LT.1 $\phi$ ) GO TO 188 - The adjustment of TPRINT is done every tenth print-out. When IFLAG<sup>4</sup> = 1 $\phi$ , then it sets it back to  $\phi$  and advances IFLAG<sup>5</sup> by 1. IFLAG<sup>5</sup> is treated as the first significant digit, so it gets reset to zero when it reaches ten.

HMIN=TPRINT

. . .

18 $\phi$  CONTINUE - This determines HMIN, the minimum average step-size (HBAR) over the previous print interval.

IF(HMIN/TPRINT.LT. $\phi.\phi\phi 1$ ) GO TO 188 - If more than 1000 steps were required at any altitude during the previous print interval, then

the next section is skipped, i.e., TPRINT is not adjusted. If less than 1000 steps were required, then TPRINT will be adjusted, so it goes to

IF(ALPHA.LT.90.0.OR.ALPHA.GT.90.0+SQRTF(Z(1))) GO TO 182 - If  $\alpha < 90$  or  $\alpha > 90 + \sqrt{Z}$ , then the altitudes of interest are either in total daylight or total darkness. If neither is true, then the region is in twilight. The following section, i.e.,

IF(TPRINT\*10.0.LT.TMAX2) GO TO 184

...

184 TPRINT=TPRINT\*10.0 - Increase TPRINT either by X10 or up to TMAX1 (whichever is smaller) for daylight or dark conditions, or increase TPRINT either by X10 or up to TMAX2 (whichever is smaller) for twilight conditions. (TMAX1 and TMAX2 are the input upper limits for TPRINT). Then

IFLAG4=IFLAG5

IFLAG5=0

GO TO 190 - which shifts the identities of the first and second significant digits in T, and goes to statement #190.

188 IF(ALPHA.GT.90.AND.ALPHA.LT.90.0+SQRTF(Z(1)).AND.TPRINT.GT.TMAX2) TPRINT=TMAX2 - This statement was reached either when it was not yet time to check on the adjustment of TPRINT (3 statements after #175) or when the average step-size was too small to increase TPRINT (one statement past #180). In either case, this statement checks to see if the sun has entered the twilight region, and if it has, decreases TPRINT if need be down to TMAX2.

190 DO 210 JZ4=1,JZEND

...

210 CONTINUE - YHOLD is shifted into YLAST so that YLAST will be available at the next print-out for checking on steady-state.

DO 220 JZ5=1,JZEND

IF(JPULL(JZ5).EQ.0) GO TO 10



220 CONTINUE - JZPULL(JZ5) was set =1 if all the species at that altitudes were at steady-state. If any of the JZPULL's are not =1, then it goes back to statement #10 to start another set of calculations. If all the JZPULL's are =1, then it winds up at

700 PRINT 999

GO TO 9000 - Which prints out a statement that "ALL SPECIES AT ALL ALTITUDES ARE NOW IN EQUILIBRIUM" and quits.

#### 4. CONCLUSION

In this report we have given the details of the use of a computer program designed to give solutions of sets of reactions. The main virtue of the program is its generality and the ease with which different reactions can be used.

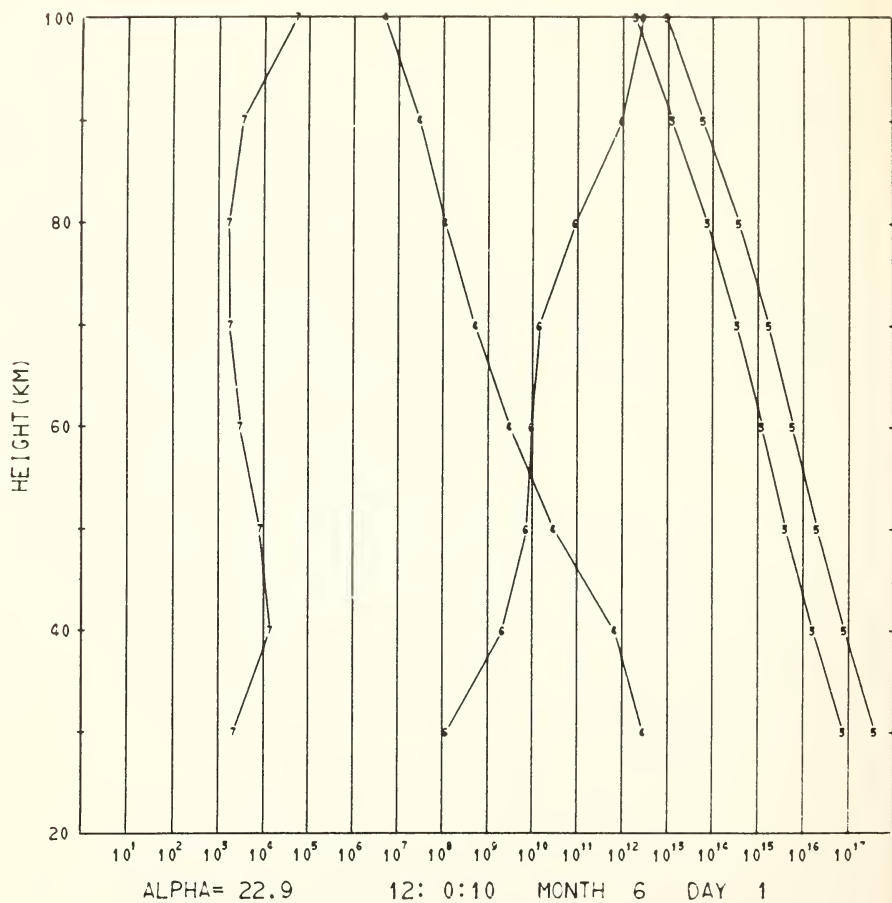


Figure 1. Sample microfilm plot.

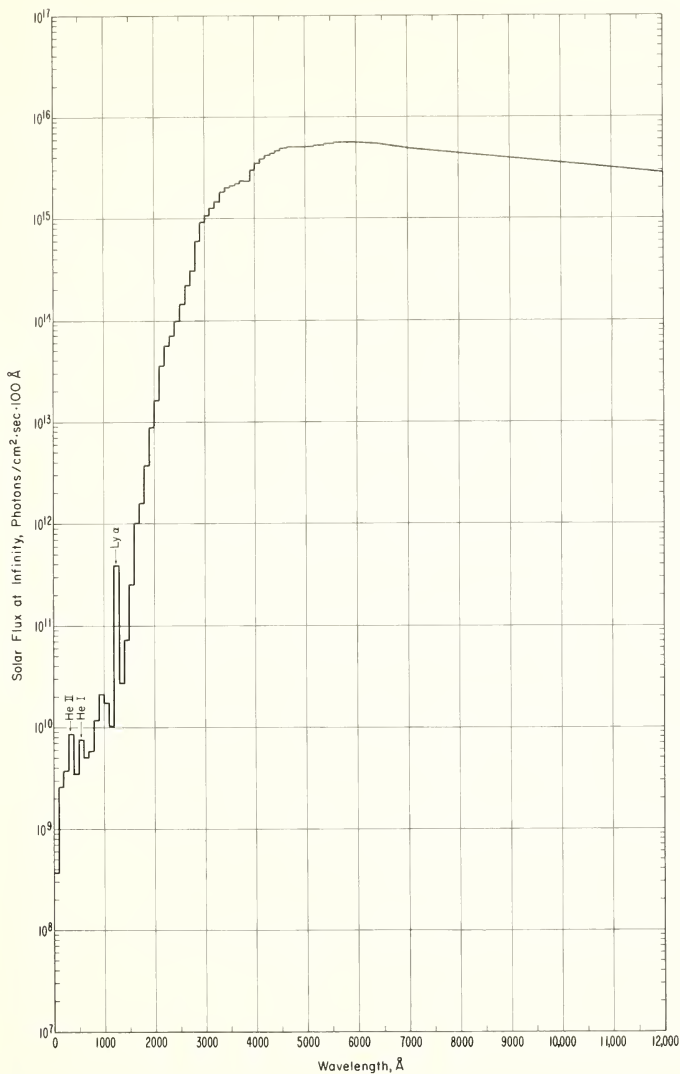


Figure 2. Solar photon flux outside the atmosphere. (These data are also tabulated in table 1.)

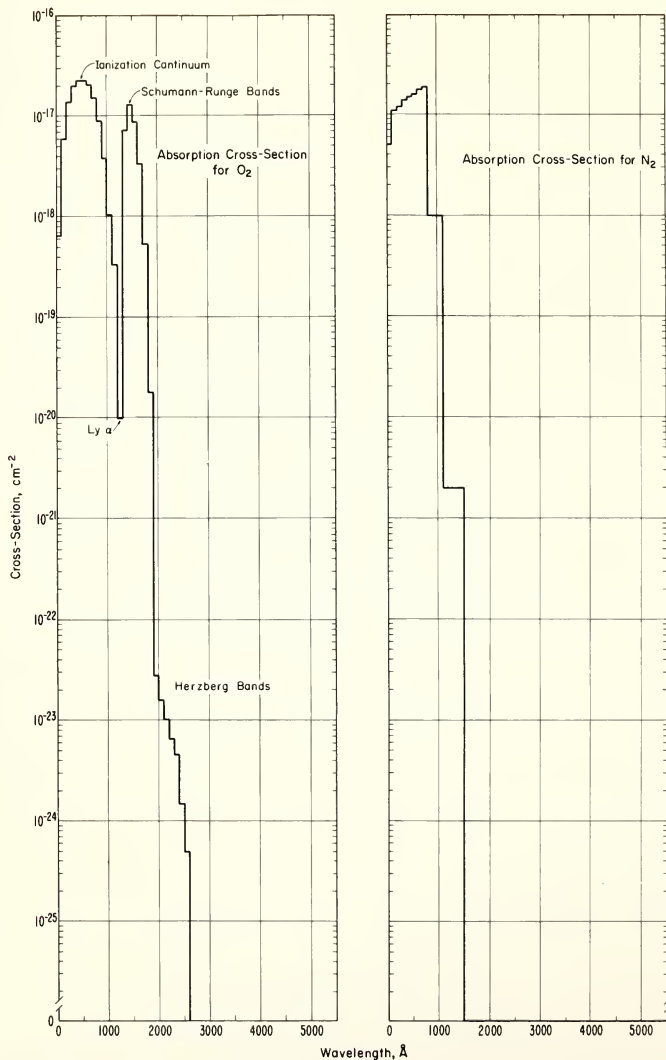


Figure 3. Absorption cross sections for  $N_2$  and  $O_2$ . (These data also tabulated in table 1.)

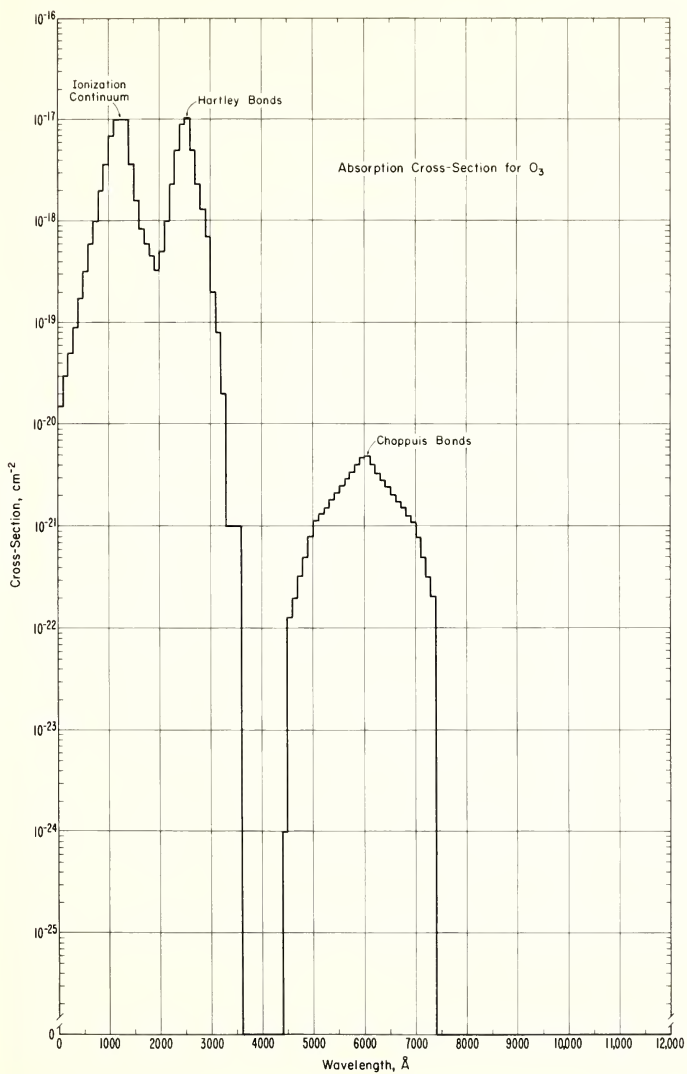


Figure 4. Absorption cross sections for  $O_3$ . (These data are also tabulated in table 1.)

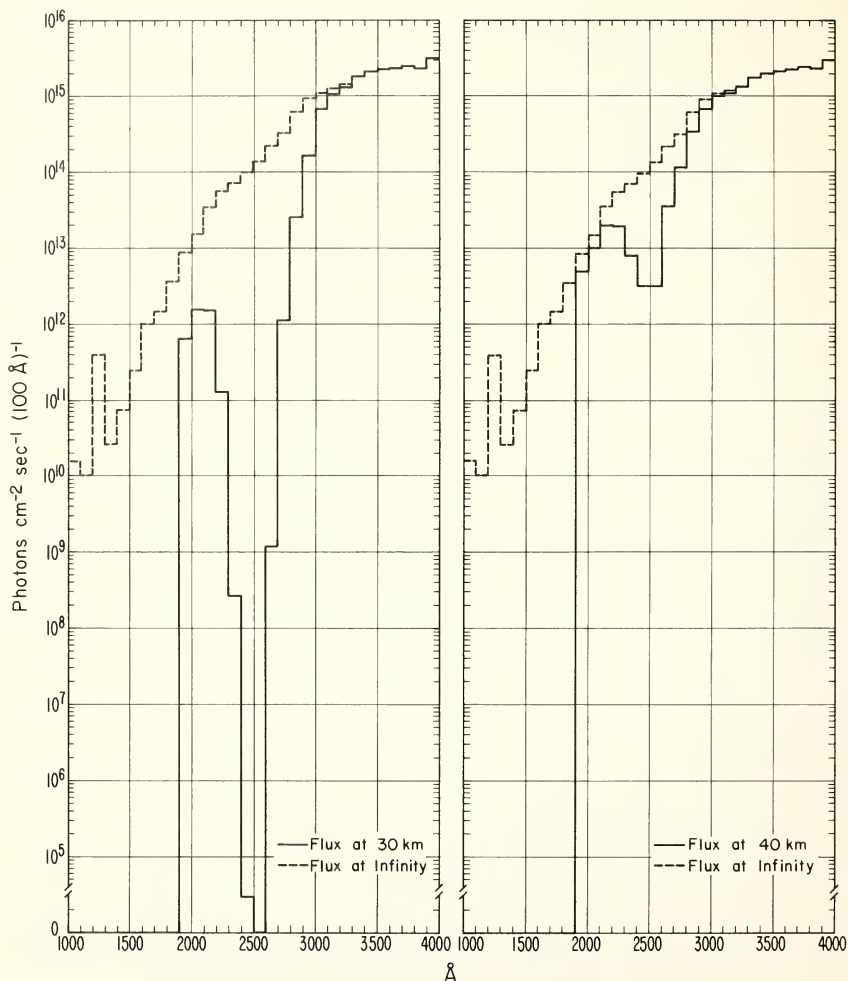


Figure 5. Solar photon flux at 30 and 40 km in the Earth's atmosphere for an overhead sun. Also shown is the flux outside the atmosphere from figure 2.

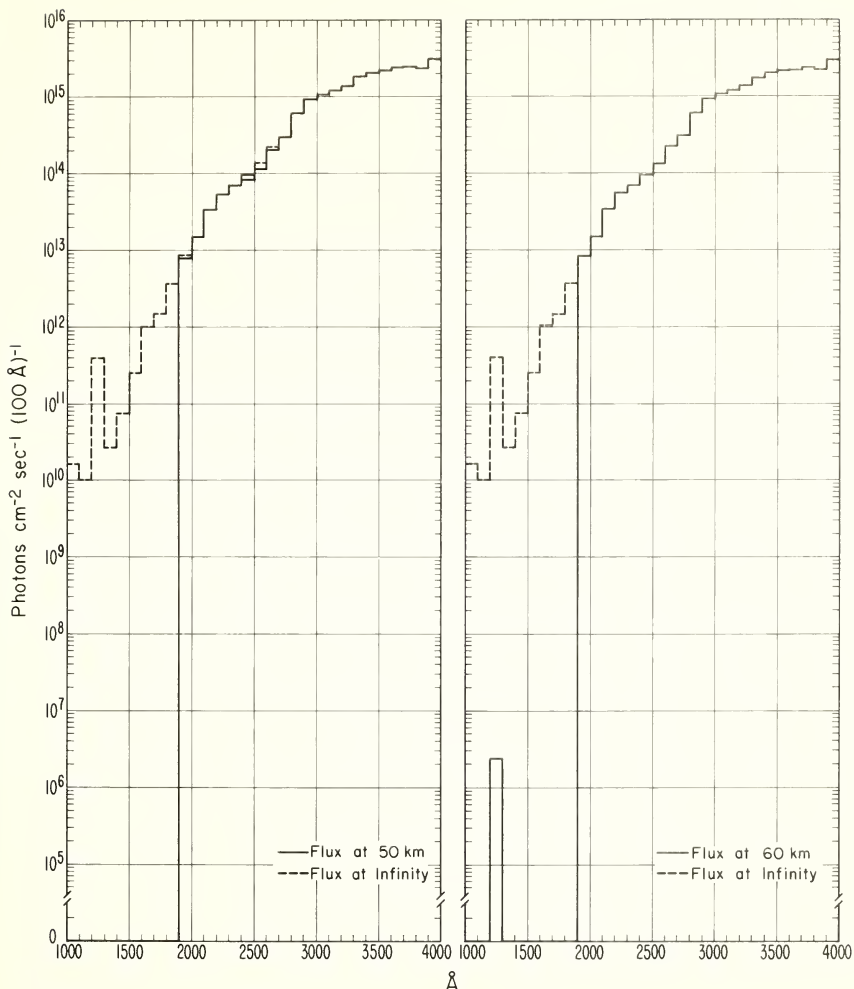


Figure 6. Solar photon flux at 50 and 60 km in the Earth's atmosphere for an overhead sun. Also shown is the flux outside the atmosphere from figure 2.

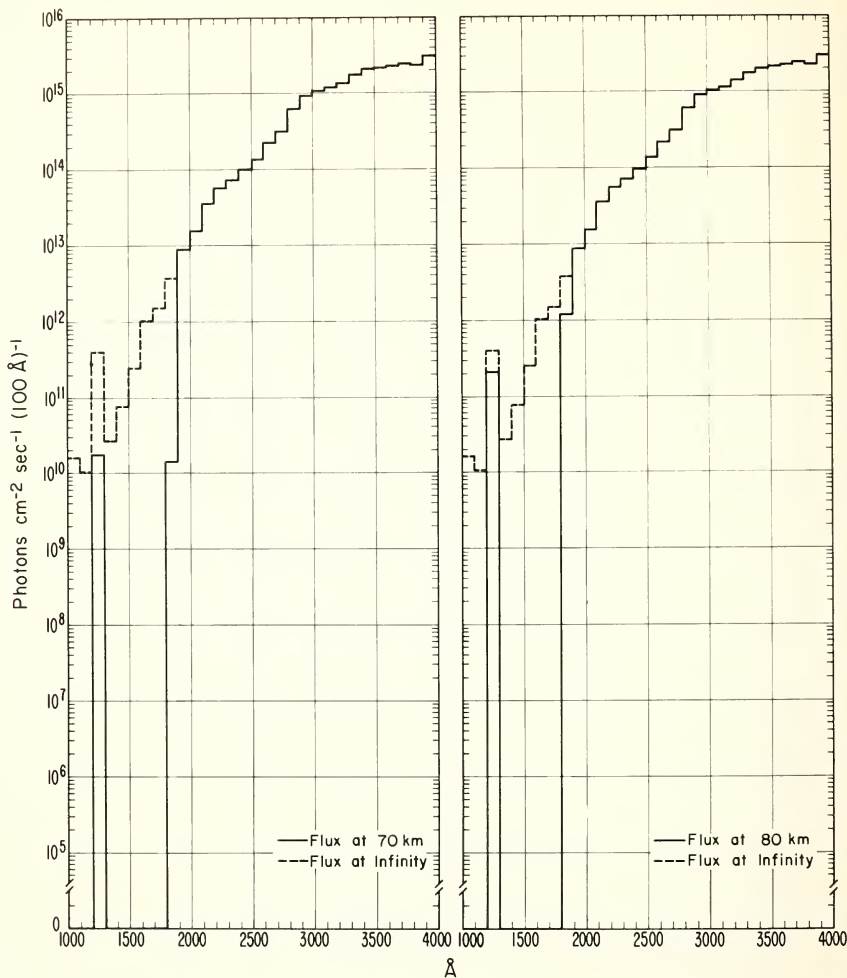


Figure 7. Solar photon flux at 70 and 80 km in the Earth's atmosphere for an overhead sun. Also shown is the flux outside the atmosphere from figure 2.



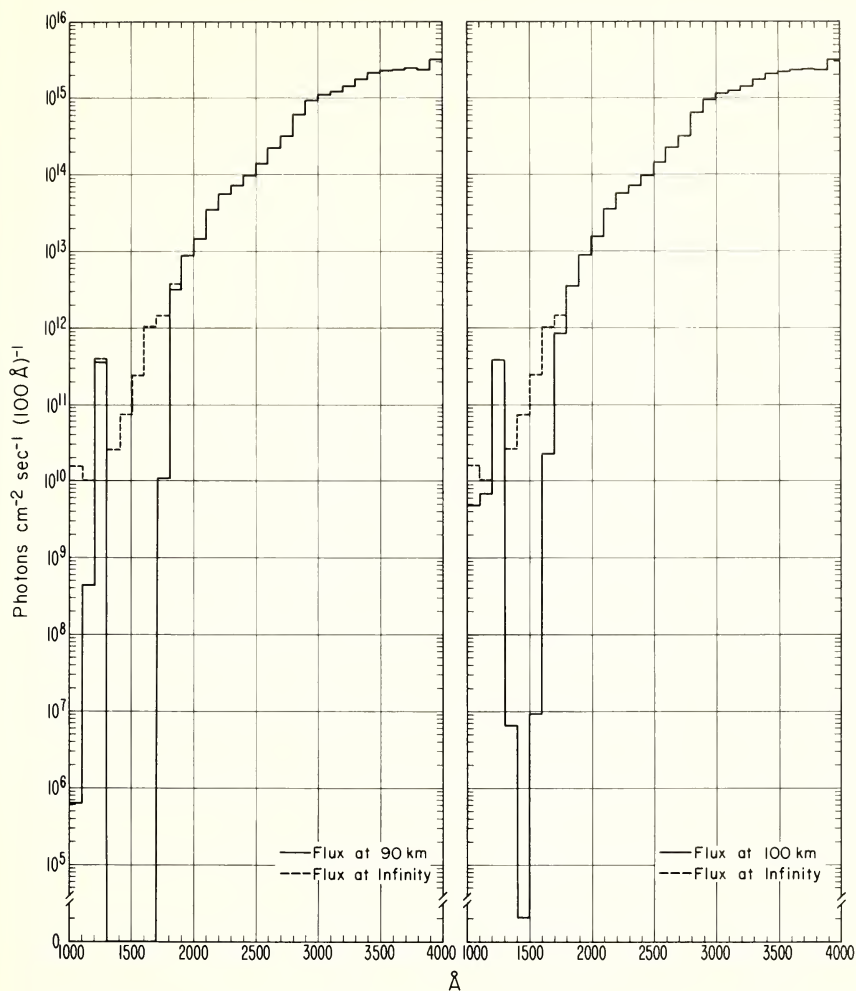


Figure 8. Solar photon flux at 90 and 100 km in the Earth's atmosphere for an overhead sun. Also shown is the flux outside the atmosphere from figure 2.

Table 1. Internal Data \*

Wavelength Band(Å)	Solar Photon Flux Outside the Atmosphere (photons/cm <sup>2</sup> -sec-100Å)	Absorption Coefficients (cm <sup>2</sup> /100Å)		
		N <sub>2</sub>	O <sub>2</sub>	O <sub>3</sub>
0-100	3.79(8)	5.0(-18)	6.0(-19)	1.5(-20)
100-200	2.65(9)	1.1(-17)	6.0(-18)	3.0(-20)
200-300	3.80(9)	1.2(-17)	1.4(-17)	5.0(-20)
300-400	8.83(9)	1.4(-17)	2.0(-17)	9.0(-20)
400-500	3.52(9)	1.5(-17)	2.3(-17)	1.7(-19)
500-600	7.71(9)	1.6(-17)	2.3(-17)	3.2(-19)
600-700	5.08(9)	1.8(-17)	2.1(-17)	6.0(-19)
700-800	5.88(9)	1.9(-17)	1.5(-17)	1.0(-18)
800-900	1.20(10)	1.0(-18)	9.0(-18)	2.0(-18)
900-1000	2.16(10)	1.0(-18)	3.8(-18)	3.6(-18)
1000-1100	1.75(10)	1.0(-18)	1.1(-18)	7.0(-18)
1100-1200	1.03(10)	2.0(-21)	3.4(-19)	1.0(-17)
1200-1300	3.94(11)	2.0(-21)	1.0(-20)	1.0(-17)
1300-1400	2.72(10)	2.0(-21)	7.2(-18)	1.0(-17)
1400-1500	7.30(10)	2.0(-21)	1.3(-17)	3.6(-18)
1500-1600	2.54(11)	0.0	8.8(-18)	1.6(-18)
1600-1700	1.03(12)	0.0	3.3(-18)	8.3(-19)
1700-1800	1.59(12)	0.0	5.3(-19)	6.0(-19)
1800-1900	3.74(12)	0.0	1.8(-20)	4.5(-19)
1900-2000	8.88(12)	0.0	2.8(-23)	3.2(-19)
2000-2100	1.64(13)	0.0	1.6(-23)	5.0(-19)
2100-2200	3.58(13)	0.0	1.0(-23)	1.0(-18)
2200-2300	5.68(13)	0.0	6.6(-24)	2.3(-18)
2300-2400	7.10(13)	0.0	4.7(-24)	5.0(-18)
2400-2500	9.90(13)	0.0	1.5(-24)	9.0(-18)
2500-2600	1.45(14)	0.0	5.0(-25)	1.0(-17)
2600-2700	2.21(14)	0.0	0.0	5.0(-18)
2700-2800	3.12(14)	0.0	0.0	2.3(-18)
2800-2900	6.12(14)	0.0	0.0	1.3(-18)
2900-3000	9.38(14)	0.0	0.0	7.0(-19)
3000-3100	1.09(15)	0.0	0.0	2.0(-19)
3100-3200	1.27(15)	0.0	0.0	8.0(-20)
3200-3300	1.49(15)	0.0	0.0	2.0(-20)
3300-3400	1.83(15)	0.0	0.0	1.0(-21)
3400-3500	2.05(15)	0.0	0.0	1.0(-21)
3500-3600	2.12(15)	0.0	0.0	1.0(-21)
3600-3700	2.23(15)	0.0	0.0	0.0
3700-3800	2.40(15)	0.0	0.0	0.0
3800-3900	2.36(15)	0.0	0.0	0.0
3900-4000	3.06(15)	0.0	0.0	0.0

Table 1. Internal Data (Cont'd)

Wavelength Band(Å)	Solar Photon Flux Outside the Atmosphere (photons/cm <sup>2</sup> -sec-100Å)	Absorption Coefficients (cm <sup>2</sup> /100Å)		
		N <sub>2</sub>	O <sub>2</sub>	O <sub>3</sub>
4000-4100	3.53(15)	0.0	0.0	0.0
4100-4200	3.93(15)	0.0	0.0	0.0
4200-4300	4.25(15)	0.0	0.0	0.0
4300-4400	4.45(15)	0.0	0.0	0.0
4400-4500	4.73(15)	0.0	0.0	1.0(-24)
4500-4600	4.94(15)	0.0	0.0	1.3(-22)
4600-4700	5.00(15)	0.0	0.0	2.0(-22)
4700-4800	5.20(15)	0.0	0.0	3.3(-22)
4800-4900	5.20(15)	0.0	0.0	5.0(-22)
4900-5000	5.20(15)	0.0	0.0	8.0(-22)
5000-5100	5.20(15)	0.0	0.0	1.1(-21)
5100-5200	5.20(15)	0.0	0.0	1.3(-21)
5200-5300	5.30(15)	0.0	0.0	1.5(-21)
5300-5400	5.30(15)	0.0	0.0	1.8(-21)
5400-5500	5.40(15)	0.0	0.0	2.1(-21)
5500-5600	5.40(15)	0.0	0.0	2.5(-21)
5600-5700	5.40(15)	0.0	0.0	2.9(-21)
5700-5800	5.40(15)	0.0	0.0	3.4(-21)
5800-5900	5.40(15)	0.0	0.0	4.0(-21)
5900-6000	5.40(15)	0.0	0.0	4.7(-21)
6000-6100	5.40(15)	0.0	0.0	4.8(-21)
6100-6200	5.40(15)	0.0	0.0	4.0(-21)
6200-6300	5.40(15)	0.0	0.0	3.3(-21)
6300-6400	5.35(15)	0.0	0.0	2.8(-21)
6400-6500	5.35(15)	0.0	0.0	2.4(-21)
6500-6600	5.30(15)	0.0	0.0	2.0(-21)
6600-6700	5.25(15)	0.0	0.0	1.7(-21)
6700-6800	5.20(15)	0.0	0.0	1.5(-21)
6800-6900	5.15(15)	0.0	0.0	1.2(-21)
6900-7000	5.10(15)	0.0	0.0	1.1(-21)
7000-7100	5.05(15)	0.0	0.0	7.8(-22)
7100-7200	5.00(15)	0.0	0.0	5.0(-22)
7200-7300	4.95(15)	0.0	0.0	3.2(-22)
7300-7400	4.90(15)	0.0	0.0	2.0(-22)
7400-7500	4.85(15)	0.0	0.0	0.0
7500-7600	4.80(15)	0.0	0.0	0.0
7600-7700	4.72(15)	0.0	0.0	0.0
7700-7800	4.64(15)	0.0	0.0	0.0
7800-7900	4.56(15)	0.0	0.0	0.0
7900-8000	4.48(15)	0.0	0.0	0.0
8000-8100	4.44(15)	0.0	0.0	0.0
8100-8200	4.39(15)	0.0	0.0	0.0
8200-8300	4.34(15)	0.0	0.0	0.0
8300-8400	4.30(15)	0.0	0.0	0.0

Table 1. Internal Data (Cont'd)

Wavelength Band(Å)	Solar Photon Flux Outside the Atmosphere (photons/cm <sup>2</sup> -sec-100Å)	Absorption Coefficients (cm <sup>2</sup> /100Å)		
		N <sub>2</sub>	O <sub>2</sub>	O <sub>3</sub>
8400-8500	4.25(15)	0.0	0.0	0.0
8500-8600	4.21(15)	0.0	0.0	0.0
8600-8700	4.17(15)	0.0	0.0	0.0
8700-8800	4.13(15)	0.0	0.0	0.0
8800-8900	4.09(15)	0.0	0.0	0.0
8900-9000	4.05(15)	0.0	0.0	0.0
9000-9100	4.00(15)	0.0	0.0	0.0
9100-9200	3.95(15)	0.0	0.0	0.0
9200-9300	3.90(15)	0.0	0.0	0.0
9300-9400	3.85(15)	0.0	0.0	0.0
9400-9500	3.80(15)	0.0	0.0	0.0
9500-9600	3.77(15)	0.0	0.0	0.0
9600-9700	3.74(15)	0.0	0.0	0.0
9700-9800	3.71(15)	0.0	0.0	0.0
9800-9900	3.68(15)	0.0	0.0	0.0
9900-10000	3.65(15)	0.0	0.0	0.0
10000-10100	3.62(15)	0.0	0.0	0.0
10100-10200	3.58(15)	0.0	0.0	0.0
10200-10300	3.54(15)	0.0	0.0	0.0
10300-10400	3.50(15)	0.0	0.0	0.0
10400-10500	3.46(15)	0.0	0.0	0.0
10500-10600	3.42(15)	0.0	0.0	0.0
10600-10700	3.39(15)	0.0	0.0	0.0
10700-10800	3.36(15)	0.0	0.0	0.0
10800-10900	3.33(15)	0.0	0.0	0.0
10900-11000	3.30(15)	0.0	0.0	0.0
11000-11100	3.26(15)	0.0	0.0	0.0
11100-11200	3.22(15)	0.0	0.0	0.0
11200-11300	3.18(15)	0.0	0.0	0.0
11300-11400	3.14(15)	0.0	0.0	0.0
11400-11500	3.10(15)	0.0	0.0	0.0
11500-11600	3.06(15)	0.0	0.0	0.0
11600-11700	3.01(15)	0.0	0.0	0.0
11700-11800	2.97(15)	0.0	0.0	0.0
11800-11900	2.93(15)	0.0	0.0	0.0
11900-12000	2.88(15)	0.0	0.0	0.0

\* after Allen, 1963.

## 5. REFERENCES

- Allen, C. W. (1963), *Astrophysical Quantities*, 2nd ed., University of London, The Athlone Press.
- Hunt, B. G. (1966), Photochemistry of ozone in a moist atmosphere, *J. Geophys. Res.*, 71, 1385-1398.
- Kenesha, T. J. (1962), A computer program for solving the reaction rate equations in the E ionospheric region, AFCRL Res. Rpt. 62-828.
- Kenesha, T. J. (1963), A solution to the reaction rate equations in the atmosphere below 150 kilometers, AFCRL Res. Rpt. 63-711.
- Kenesha, T. J. (1967), A technique for solving the general reaction-rate equations in the atmosphere, AFCRL Res. Rpt. 67-0221.
- Romanelli, J. J. (1964), Runge-Kutta methods for the solution of ordinary differential equations, in *Mathematical Methods for Digital Computers*, A Ralston and H. S. Wilf, editors, John Wiley and Sons, New York.
- Swider, W., Jr. (1964), The determination of the optical depth at large solar zenith distances, *Planet. Space Sci.*, 12, 761-782.

## APPENDIX A. SAMPLE INPUT DECK

```

1
  THIS IS HUNTS REACTION SET, CHANGED TO EXTEND THE SOLAR FLUX DOWN THROUGH
  THE UV, WITH THE DEACTIVATION OF OLD INCREASED TO 1.0E-10, AND EQUIL 1.E-8
  RUN FIRST TO STEADY STATE, AND THEN RESTART WITH JOSHUA AT 0 AT LAT 90.0 DEG
06 03 05 04 05 01 8.00E-35 3.00E+02 +0.00E+00 +4.45E+02
06 04 01 03 03 01 5.60E-11 3.00E+02 +0.00E+00 -2.85E+03
06 06 05 03 05 01 2.70E-33 3.00E+02 +0.00E+00 +0.00E+00
07 04 01 03 03 01 1.00E-11 3.00E+02 +0.00E+00 +0.00E+00
07 05 01 06 05 01 1.00E-10 3.00E+02 +0.00E+00 +0.00E+00
08 04 01 09 03 01 2.60E-11 3.00E+02 +0.00E+00 +0.00E+00
09 06 01 08 03 01 5.00E-11 3.00E+02 +0.00E+00 +0.00E+00
09 04 01 10 03 01 5.00E-13 3.00E+02 +0.00E+00 +0.00E+00
09 09 01 11 06 01 2.80E-12 3.00E+02 +0.00E+00 +0.00E+00
09 10 01 11 03 01 1.00E-11 3.00E+02 +0.00E+00 +0.00E+00
08 10 01 12 03 01 2.00E-13 3.00E+02 +0.00E+00 +0.00E+00
08 10 01 09 09 01 1.00E-11 3.00E+02 +0.00E+00 +0.00E+00
06 10 01 09 03 01 1.00E-11 3.00E+02 +0.00E+00 +0.00E+00
08 03 05 10 05 01 7.40E-32 3.00E+02 +0.00E+00 +0.00E+00
08 09 05 11 05 01 2.50E-31 3.00E+02 +0.00E+00 +0.00E+00
08 08 05 12 05 01 2.60E-32 3.00E+02 +0.00E+00 +0.00E+00
10 10 01 13 03 01 3.00E-12 3.00E+02 +0.00E+00 +0.00E+00
09 13 01 11 10 01 4.00E-13 3.00E+02 +0.00E+00 +0.00E+00
06 13 01 09 10 01 1.00E-15 3.00E+02 +0.00E+00 +0.00E+00
08 13 01 12 10 01 1.00E-13 3.00E+02 +0.00E+00 +0.00E+00
07 12 01 09 08 01 1.00E-11 3.00E+02 +0.00E+00 +0.00E+00
07 11 01 09 09 01 1.00E-11 3.00E+02 +0.00E+00 +0.00E+00
06 09 05 10 05 01 1.40E-31 3.00E+02 +0.00E+00 +0.00E+00
10 04 01 09 03 03 1.00E-14 3.00E+02 +0.00E+00 +0.00E+00
99
03 01 01 06 06 01
018 025
2.65E-19 1.80E-20 2.80E-23 1.60E-23 1.00E-23 6.60E-24 4.60E-24
3.75E-25
03 01 01 06 07 01
012 018
3.40E-19 1.00E-20 7.20E-18 1.30E-17 8.80E-18 3.30E-18 2.65E-19
03 01 01 07 07 01
001 011
6.00E-19 6.00E-18 1.40E-17 2.00E-17 2.30E-17 2.30E-17 2.10E-17
1.50E-17 9.00E-18 3.80E-18 1.10E-18
04 01 01 03 06 01
032 074
8.00E-20 2.00E-20 1.00E-21 1.00E-21 1.00E-21 0.00E+00 0.00E+00
0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 1.00E-24
1.30E-22 2.00E-22 3.30E-22 5.00E-22 8.00E-22 1.13E-21 1.30E-21
1.50E-21 1.80E-21 2.10E-21 2.50E-21 2.90E-21 3.35E-21 4.00E-21
4.65E-21 4.80E-21 4.00E-21 3.25E-21 2.80E-21 2.40E-21 2.00E-21
1.70E-21 1.50E-21 1.25E-21 1.08E-21 7.80E-22 5.00E-22 3.20E-22
2.05E-22
04 01 01 07 03 01
001 031
1.50E-20 3.00E-20 5.00E-20 9.00E-20 1.70E-19 3.20E-19 6.00E-19
1.00E-18 2.00E-18 3.60E-18 7.00E-18 1.00E-17 1.00E-17 1.00E-17
3.60E-18 1.60E-18 8.30E-19 6.00E-19 4.50E-19 3.20E-19 5.00E-19
1.00E-18 2.30E-18 5.00E-18 9.00E-18 1.00E-17 5.00E-18 2.30E-18
1.30E-18 7.00E-19 2.00E-19
11 01 01 09 08 01
002 019
1.00E-18 1.00E-17 2.00E-17 1.30E-17 1.50E-17 1.80E-17 1.20E-17
1.00E-17 1.00E-17 8.00E-18 5.00E-18 1.40E-17 3.00E-18 7.00E-19
2.00E-18 4.00E-18 2.00E-18 2.00E-19
13 01 01 09 09 01

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002 030
1.00E-18 1.00E-17 2.00E-17 1.30E-17 1.50E-17 1.80E-17 1.20E-17
1.00E-17 1.00E-17 8.00E-18 5.00E-18 1.40E-17 3.00E-18 7.00E-19
2.00E-18 4.00E-18 2.00E-18 1.40E-18 7.00E-19 4.70E-19 3.50E-19
2.60E-19 1.80E-19 1.50E-19 1.00E-19 5.00E-20 3.00E-20 2.00E-20
1.60E-20
99
00 1.000E+02 3.000E+01 1.000E+01
2.12E+02 1.81E+02 1.85E+02 2.17E+02 2.58E+02 2.70E+02 2.48E+02
2.28E+02
03 0 2
04 0 3
05 0 0
06 0 1
07 0 1
08 1 1
09 1 2
10 1 3
11 2 3
12 2 2
13 2 4
0.00E+00 1.80E+03 1.30E+06 2.59E+05 3.30E+07 1 0 1.00E-08 0
+9.00E+01 +0.00E+00 09 22 12 00 00
3
3.64+012 1.32+013 8.07+013 3.68+014 1.27+015 4.26+015 1.69+016
7.66+016 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
4
8.21+006 3.57+007 1.74+008 5.04+008 1.26+010 1.17+011 1.41+012
2.89+012 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
5
9.98+012 6.48+013 4.03+014 1.84+015 6.33+015 2.13+016 8.46+016
3.83+017 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
6
3.34+012 8.69+011 5.58+010 8.47+009 2.22+010 1.10+010 1.62+009
7.50+007 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
7
1.11+002 4.12+001 2.92+001 1.71+001 1.16+002 1.70+002 6.37+001
4.35+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
8
9.95+007 4.75+008 9.07+007 7.92+006 1.58+006 1.83+005 1.07+003
1.15+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
9
1.29+002 1.09+004 2.26+005 1.19+006 1.32+006 3.24+006 1.89+006
6.88+005 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
10
8.00+000 3.49+003 3.92+005 4.71+006 4.29+006 1.27+007 4.72+007
3.35+007 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
11
1.50+002 1.71+002 7.35+005 6.67+009 3.07+010 1.52+011 8.05+011
1.51+012 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
12
4.30+005 1.99+008 3.11+009 4.45+009 4.88+008 1.88+008 5.26+007
8.72+005 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
13
5.50+008 3.56+002 2.41+003 4.94+005 3.87+005 5.67+006 5.97+008
6.91+009 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000 0.00+000
99
11

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APPENDIX B. SIXBIT OUTPUT FOR THE INPUT SHOWN IN APPENDIX A.

THIS IS HUNTS REACTION SET, CHANGED TO EXTEND THE SOLAR FLUX DOWN THROUGH THE UV, WITH THE DEACTIVATION OF OLD INCREASED TO  $1.0E-10$ , AND EQUIL  $1.E-8$

RUN FIRST TO STEADY STATE, AND THEN RESTART WITH JOSHUA AT 0 AT LAT 85.0 DEG THERE HAVE BEEN 24 REACTIONS INPUT INVOLVING 11 SPECIES. THE REACTIONS AND THEIR RATE COEFFICIENTS ARE

1	6+ 3+ 5--- 4+ 5+ 1	$K = 8.00-035*(TEMP/3.00+002)** 0.00*EXP( 4.45+002/TEMP)$
2	6+ 4+ 1--- 3+ 3+ 1	$K = 5.60-011*(TEMP/3.00+002)** 0.00*EXP(-2.85+003/TEMP)$
3	6+ 6+ 5--- 3+ 5+ 1	$K = 2.70-033*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
4	7+ 4+ 1--- 3+ 3+ 1	$K = 1.00-011*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
5	7+ 5+ 1--- 6+ 5+ 1	$K = 1.00-010*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
6	8+ 4+ 1--- 9+ 3+ 1	$K = 2.60-011*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
7	9+ 6+ 1--- 8+ 3+ 1	$K = 5.00-011*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
8	9+ 4+ 1---10+ 3+ 1	$K = 5.00-013*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
9	9+ 9+ 1---11+ 6+ 1	$K = 2.80-012*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
10	9+10+ 1---11+ 3+ 1	$K = 1.00-011*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
11	9+10+ 1---12+ 3+ 1	$K = 2.00-013*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
12	8+10+ 1--- 9+ 9+ 1	$K = 1.00-011*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$
13	6+10+ 1--- 9+ 3+ 1	$K = 1.00-011*(TEMP/3.00+002)** 0.00*EXP( 0.00+000/TEMP)$



14    8+ 3+ 5---10+ 5+ 1    K = 7.40-032\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 15    8+ 9+ 5---11+ 5+ 1    K = 2.50-031\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 16    8+ 8+ 5---12+ 5+ 1    K = 2.60-032\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 17    10+10+ 1---13+ 3+ 1    K = 3.00-012\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 18    9+13+ 1---11+10+ 1    K = 4.00-013\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 19    6+13+ 1--- 9+10+ 1    K = 1.00-015\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 20    8+13+ 1---12+10+ 1    K = 1.00-013\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 21    7+12+ 1--- 9+ 8+ 1    K = 1.00-011\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 22    7+11+ 1--- 9+ 9+ 1    K = 1.00-011\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 23    6+ 9+ 5---10+ 5+ 1    K = 1.40-031\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)  
 24    10+ 4+ 1--- 9+ 3+ 3    K = 1.00-014\*(TEMP/3.00+002)\*\* 0.00\*EXP( 0.00+000/TEMP)

THERE HAVE BEEN 7 PHOTOREACTIONS INPUT.

25    3+ PHOTON --- 6+ 6+ 1

26    3+ PHOTON --- 6+ 7+ 1

27    3+ PHOTON --- 7+ 7+ 1

28      4+ PHOTON --- 3+ 6+ 1

29      4+ PHOTON --- 7+ 3+ 1

30      11+ PHOTON --- 9+ 8+ 1

31      13+ PHOTON --- 9+ 9+ 1

-----STARTING VALUES-----  
 REACTION TERM BLOCK CONTAINS RATE COEFFICIENTS

LOCAL TIME (HOURS,MINUTES,SECONDS) = 12/00/00 ON DAY NUMBER 22, MONTH NUMBER 6  
 COMPUTER TIME = 135.641 SECONDS  
 RUNNING TIME = 0.000+000 SECONDS  
 ZENITH ANGLE = 65.27 DEGREES, LATITUDE = 85.00LONGITUDE = 0.00

REACTION TERMS-----

HEIGHT	STEP SIZE	TERM(1)	TERM(2)	TERM(3)	TERM(4)	TERM(5)	TERM(6)	TERM(7)
		TERM(8)	TERM(9)	TERM(10)	TERM(11)	TERM(12)	TERM(13)	TERM(14)
		TERM(15)	TERM(16)	TERM(17)	TERM(18)	TERM(19)	TERM(20)	TERM(21)
		TERM(24)	TERM(25)	TERM(26)	TERM(27)	TERM(28)	TERM(29)	TERM(30)
								TERM(31)
100.0	1.0000+000	6.527-034	8.124-017	2.700-033	1.000-011	1.000-010	2.600-011	5.000-011
	5.000-013	2.800-012	1.000-011	2.000-013	1.000-011	1.000-011	7.400-032	2.500-031
	2.600-032	3.000-012	4.000-013	1.000-013	1.000-015	1.000-013	1.000-011	1.400-031
	1.000-014	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000
90.0	1.0000+000	9.350-034	8.125-018	2.700-033	1.000-011	1.000-010	2.600-011	5.000-011
	5.000-013	2.800-012	1.000-011	2.000-013	1.000-011	1.000-011	7.400-032	2.500-031
	2.600-032	3.000-012	4.000-013	1.000-013	1.000-015	1.000-013	1.000-011	1.400-031
	1.000-014	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000
80.0	1.0000+000	8.866-034	1.142-017	2.700-033	1.000-011	1.000-010	2.600-011	5.000-011
	5.000-013	2.800-012	1.000-011	2.000-013	1.000-011	1.000-011	7.400-032	2.500-031
	2.600-032	3.000-012	4.000-013	1.000-013	1.000-015	1.000-013	1.000-011	1.400-031
	1.000-014	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000
70.0	1.0000+000	6.219-034	1.107-016	2.700-033	1.000-011	1.000-010	2.600-011	5.000-011
	5.000-013	2.800-012	1.000-011	2.000-013	1.000-011	1.000-011	7.400-032	2.500-031
	2.600-032	3.000-012	4.000-013	1.000-013	1.000-015	1.000-013	1.000-011	1.400-031
	1.000-014	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000
60.0	1.0000+000	4.489-034	8.928-016	2.700-033	1.000-011	1.000-010	2.600-011	5.000-011
	5.000-013	2.800-012	1.000-011	2.000-013	1.000-011	1.000-011	7.400-032	2.500-031
	2.600-032	3.000-012	4.000-013	1.000-013	1.000-015	1.000-013	1.000-011	1.400-031
	1.000-014	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000
50.0	1.0000+000	4.158-034	1.459-015	2.700-033	1.000-011	1.000-010	2.600-011	5.000-011
	5.000-013	2.800-012	1.000-011	2.000-013	1.000-011	1.000-011	7.400-032	2.500-031
	2.600-032	3.000-012	4.000-013	1.000-013	1.000-015	1.000-013	1.000-011	1.400-031
	1.000-014	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000
40.0	1.0000+000	4.812-034	5.719-016	2.700-033	1.000-011	1.000-010	2.600-011	5.000-011
	5.000-013	2.800-012	1.000-011	2.000-013	1.000-011	1.000-011	7.400-032	2.500-031
	2.600-032	3.000-012	4.000-013	1.000-013	1.000-015	1.000-013	1.000-011	1.400-031
	1.000-014	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000
30.0	1.0000+000	5.633-034	2.087-016	2.700-033	1.000-011	1.000-010	2.600-011	5.000-011
	5.000-013	2.800-012	1.000-011	2.000-013	1.000-011	1.000-011	7.400-032	2.500-031
	2.600-032	3.000-012	4.000-013	1.000-013	1.000-015	1.000-013	1.000-011	1.400-031
	1.000-014	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000	0.000+000

## SPECIES DENSITIES----

HEIGHT	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)
	Y(10)	Y(11)	Y(12)	Y(13)	Y(14)	Y(15)	Y(16)	Y(17)
100.0	1.00000000 8.000+000	3.640+012 1.500+002	8.210+006 4.300+005	9.980+012 5.500+008	3.340+012 0.000+000	1.110+002 0.000+000	9.950+007 0.000+000	1.290+002 0.000+000
90.0	1.00000000 3.490+003	1.320+013 1.710+002	3.570+007 1.990+008	6.480+013 3.560+002	8.690+011 0.000+000	4.120+001 0.000+000	4.750+008 0.000+000	1.090+004 0.000+000
80.0	1.00000000 3.920+005	8.070+013 7.350+005	1.740+008 3.110+009	4.030+014 2.410+003	5.580+010 0.000+000	2.920+001 0.000+000	9.070+007 0.000+000	2.240+005 0.000+000
70.0	1.00000000 4.710+006	3.680+014 6.670+009	5.040+008 4.450+009	1.840+015 4.940+005	8.470+009 0.000+000	1.710+001 0.000+000	7.920+006 0.000+000	1.190+006 0.000+000
60.0	1.00000000 4.250+006	1.270+015 3.070+010	1.260+010 4.880+008	6.330+015 3.870+005	2.220+010 0.000+000	1.160+002 0.000+000	1.580+006 0.000+000	1.320+006 0.000+000
50.0	1.00000000 1.270+007	4.260+015 1.520+011	1.170+011 1.880+008	2.130+016 5.470+006	1.100+010 0.000+000	1.700+002 0.000+000	1.830+005 0.000+000	3.240+006 0.000+000
40.0	1.00000000 4.720+007	1.690+014 8.050+011	1.410+012 5.260+007	8.440+016 5.970+008	1.620+009 0.000+000	6.370+001 0.000+000	1.070+003 0.000+000	1.890+006 0.000+000
30.0	1.00000000 3.350+007	7.660+014 1.510+012	2.890+012 8.720+005	3.840+017 6.910+009	7.500+007 0.000+000	4.350+000 0.000+000	1.150+000 0.000+000	6.880+005 0.000+000

LOCAL TIME (HOURS:MINUTES:SECONDS) = 12/30/00 ON DAY NUMBER 22, MONTH NUMBER 6

COMPUTER TIME = 138.180 SECONDS

RUNNING TIME = 1.800+003 SECONDS

ZENITH ANGLE = 65.27 DEGREES, LATITUDE = 85.00LONGITUDE = 0.00

REACTION TERMS-----

HEIGHT	STEP	SIZE	TERM(1)	TERM(2)	TERM(3)	TERM(4)	TERM(5)	TERM(6)	TERM(7)
	TERM(16)	TERM(9)	TERM(10)	TERM(11)	TERM(12)	TERM(13)	TERM(14)	TERM(15)	
	TERM(17)	TERM(18)	TERM(19)	TERM(20)	TERM(21)	TERM(22)	TERM(23)	TERM(24)	
	TERM(24)	TERM(25)	TERM(26)	TERM(27)	TERM(28)	TERM(29)	TERM(30)	TERM(31)	
100.0	3.0000+002	7.919+004	2.226+003	3.006+005	9.077+003	1.104+005	2.122+004	2.150+004	
	5.280+004	4.639+008	1.031+008	1.594+004	7.949+003	2.675+002	2.675+002	3.196+008	
	2.569+003	1.924+010	2.838+018	1.841+010	5.488+013	4.758+004	1.660+011	6.007+004	
	6.569+007	2.663+005	5.803+004	5.733+001	3.479+003	5.226+004	8.871+008	7.764+012	
90.0	1.2000+002	6.950+005	2.563+002	1.321+005	1.518+002	2.710+005	4.482+005	4.784+005	
	1.998+001	3.393+004	3.805+004	3.283+001	1.641+001	3.004+004	3.006+004	4.667+005	
	3.799+001	3.585+005	1.508+010	2.976+005	1.626+006	8.321+002	7.151+008	8.678+002	
	1.255+003	5.703+005	3.979+004	3.227+004	1.540+004	2.312+005	8.005+004	4.739+006	
80.0	1.2000+002	1.611+006	1.125+002	3.394+003	5.246+002	1.199+006	4.153+005	6.337+005	
	1.999+001	1.441+001	8.842+001	7.064+003	3.532+002	2.177+005	2.181+005	2.071+003	
	8.603+002	4.558+001	2.160+004	1.330+001	2.157+002	9.255+001	2.187+004	7.150+001	
	6.871+001	5.765+005	7.915+004	1.286+032	7.476+004	1.120+006	1.054+000	3.156+001	
70.0	1.2000+002	3.647+006	5.011+002	3.727+002	9.360+002	3.296+006	1.091+005	5.121+005	
	3.089+002	3.915+000	5.490+001	7.455+000	3.728+002	4.021+005	4.023+005	4.767+003	
	3.083+003	6.468+001	2.313+001	4.236+000	3.927+001	7.972+001	1.195+000	2.638+000	
	2.426+001	5.857+005	1.713+003	3.638+011	2.216+005	3.305+006	4.350+001	6.361+001	
60.0	1.2000+002	8.073+002	2.550+005	8.553+003	1.499+001	7.432+007	5.277+005	1.474+006	
	8.415+003	4.865+000	5.821+001	1.356+000	6.779+001	9.453+005	9.457+005	3.416+003	
	4.159+004	5.455+001	2.031+001	8.617+000	6.123+002	5.729+001	3.604+001	2.613+001	
	5.445+002	1.912+006	1.793+005	0.000+000	5.413+006	7.442+007	6.069+007	4.683+001	
50.0	3.0000+002	4.158+008	1.888+006	6.984+003	2.000+002	3.627+008	5.571+005	1.784+006	
	1.900+005	2.933+001	4.110+002	4.634+001	2.317+001	1.400+006	1.225+006	3.144+003	
	1.843+005	4.839+002	7.323+000	6.235+001	1.032+001	3.202+001	2.589+002	1.064+003	
	1.491+004	4.444+006	3.891+034	0.000+000	4.962+007	3.630+008	1.944+035	4.223+002	
40.0	3.6000+002	1.114+009	1.305+006	5.985+002	8.968+002	5.383+008	3.919+004	1.523+005	
	1.326+006	9.909+000	8.864+002	1.008+002	5.039+001	7.627+005	1.132+005	4.255+005	
	2.516+009	6.660+003	4.482+002	9.662+002	6.384+002	3.347+002	5.122+002	3.607+001	
	6.641+005	2.424+006	9.395+011	0.000+000	5.727+008	5.383+008	6.265+012	5.333+003	
30.0	6.0000+002	1.237+009	4.515+004	5.794+000	1.258+002	1.667+008	8.589+001	2.564+003	
	9.889+005	1.312+000	2.284+002	7.429+006	3.814+004	2.498+004	2.482+003	7.694+008	
	1.302+014	3.339+003	1.882+003	5.174+002	7.900+004	3.796+005	6.573+001	2.748+000	
	9.639+005	9.573+004	0.000+000	0.000+000	1.070+009	1.667+008	0.000+000	9.838+002	

## SPECIES DENSITIES----

HEIGHT	Y(2)	Y(3)	Y(4)	Y(5)	Y(6)	Y(7)	Y(8)	Y(9)
	Y(10)	Y(11)	Y(12)	Y(13)	Y(14)	Y(15)	Y(16)	Y(17)
100.0	0.99991427 8.008+000	3.640+012 1.500+002	8.203+006 4.300+005	9.940+012 5.511+008	3.340+012 0.000+000	1.106+002 0.000+000	9.950+007 0.000+000	1.287+002 0.000+000
90.0	1.000168A2 3.457+003	1.320+013 1.710+002	3.630+007 1.990+008	6.440+013 3.423+002	8.690+011 0.000+000	4.181+001 0.000+000	4.749+008 0.000+000	1.101+004 0.000+000
80.0	1.00001062 3.897+005	8.070+013 7.350+005	1.763+008 3.110+009	4.030+014 2.380+003	5.587+010 0.000+000	2.977+001 0.000+000	9.061+007 0.000+000	2.249+005 0.000+000
70.0	0.99999515 4.632+006	3.680+014 6.670+009	5.250+008 4.450+009	1.840+015 4.478+005	8.704+009 0.000+000	1.799+001 0.000+000	8.049+006 0.000+000	1.181+006 0.000+000
60.0	0.99999900 4.262+006	1.270+015 3.070+010	1.277+010 4.880+008	6.330+015 3.851+005	2.238+010 0.000+000	1.176+002 0.000+000	1.590+006 0.000+000	1.318+006 0.000+000
50.0	0.99999815 1.269+007	4.260+015 1.520+011	1.175+011 1.890+008	2.130+016 5.456+006	1.103+010 0.000+000	1.705+002 0.000+000	1.826+005 0.000+000	3.234+006 0.000+000
40.0	0.99999838 4.708+007	1.690+016 8.050+011	1.409+012 5.260+007	8.440+016 5.968+008	1.618+009 0.000+000	6.362+001 0.000+000	1.069+003 0.000+000	1.880+006 0.000+000
30.0	0.99999770 3.326+007	7.660+014 1.510+012	2.887+012 8.720+005	3.830+017 6.910+009	7.485+007 0.000+000	4.351+000 0.000+000	1.140+000 0.000+000	6.825+005 0.000+000

MAJOR DESTRUCTION REACTIONS-----  
HEIGHT NO. 2 NO. 3 NO. 10 NO. 11 NO. 4 NO. 12 NO. 5 NO. 6 NO. 7 NO. 8 NO. 9

HEIGHT	NO. 2	NO. 3	NO. 10	NO. 11	NO. 4	NO. 12	NO. 5	NO. 6	NO. 7	NO. 8	NO. 9
100.0	0/ 0, 0 0	25/01.26,00	29/06.00,00	29/06.00,00	29/06.00,00	29/06.00,00	19/00.00,00	03/01.00,00	05/00.00,00	06/00.00,00	07/00.00,00
	13/00.00,00	30/00.00,00						0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0
90.0	0/ 0, 0 0	01/25.00,00	06/29.00,00	06/29.00,00	06/29.00,00	06/29.00,00	19/31.00,00	01/07.03,00	05/00.00,00	06/00.00,00	07/00.00,00
	13/00.00,00	30/00.00,00						0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0
80.0	0/ 0, 0 0	01/25.14,00	29/06.00,00	29/06.00,00	29/06.00,00	29/06.00,00	31/19.00,00	01/07.13,00	05/00.00,00	06/14.00,00	07/00.00,00
	13/00.00,00	30/00.00,00						0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0
70.0	0/ 0, 0 0	01/25.14,00	29/00.00,00	29/00.00,00	29/00.00,00	29/00.00,00	31/00.00,00	01/07.13,00	05/00.00,00	14/06.00,00	07/00.00,00
	13/00.00,00	30/00.00,00						0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0
60.0	0/ 0, 0 0	01/00.00,00	29/00.00,00	29/00.00,00	29/00.00,00	29/00.00,00	31/19.00,00	01/00.00,00	05/00.00,00	14/06.00,00	07/00.00,00
	13/00.00,00	22/00.00,00						0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0
50.0	0/ 0, 0 0	01/00.00,00	29/28.00,00	29/28.00,00	29/28.00,00	29/28.00,00	31/19.00,00	01/00.00,00	05/00.00,00	14/06.00,00	07/00.00,00
	13/00.00,00	22/00.00,00						0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0
40.0	0/ 0, 0 0	01/00.00,00	28/29.00,00	28/29.00,00	28/29.00,00	28/29.00,00	31/19.00,00	01/00.00,00	05/00.00,00	14/06.00,00	08/07.00,00
	13/24.00,00	22/00.00,00						0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0
30.0	0/ 0, 0 0	01/00.00,00	28/29.00,00	28/29.00,00	28/29.00,00	28/29.00,00	31/19.00,00	01/00.00,00	05/00.00,00	14/06.00,00	08/00.00,00
	24/00.00,00	22/00.00,00						0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0	0/ 0, 0 0

MAJOR PRODUCTION REACTIONS-----  
HEIGHT

	NO. 2 NO. 10	NO. 3 NO. 11	NO. 4 NO. 12	NO. 5 NO. 13	NO. 6 NO. 14	NO. 7 NO. 15	NO. 8 NO. 16	NO. 9 NO. 17
100.0	0/ 0. 0. 0	03/29,00.00	01/00,00.00	-1/-1,-1,-1	25/05,26.00	26/29,00.00	07/00,00.00	06/00,00.00
	14/00,00.00	09/15,10.00	16/00,00.00	17/00,00.00	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0
90.0	0/ 0. 0. 0	07/08,29.03	01/00,00.00	-1/-1,-1,-1	25/05,00.00	29/26,00.00	07/00,00.00	06/00,00.00
	14/00,00.00	10/09,15.00	16/11,00.00	17/00,00.00	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0
80.0	0/ 0. 0. 0	29/07,06.13	01/00,00.00	-1/-1,-1,-1	05/25,00.00	29/00,00.00	07/00,00.00	06/13,00.00
	14/00,00.00	10/09,00.00	11/00,00.00	17/00,00.00	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0
70.0	0/ 0. 0. 0	29/07,13.00	01/00,00.00	-1/-1,-1,-1	05/25,00.00	29/00,00.00	07/00,00.00	13/06,00.00
	14/00,00.00	10/00,00.00	11/00,00.00	17/00,00.00	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0
60.0	0/ 0. 0. 0	29/00,00.00	01/00,00.00	-1/-1,-1,-1	05/00,00.00	29/00,00.00	07/00,00.00	13/06,00.00
	14/00,00.00	10/00,00.00	11/00,00.00	17/00,00.00	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0
50.0	0/ 0. 0. 0	29/28,00.00	01/00,00.00	-1/-1,-1,-1	05/28,00.00	29/00,00.00	07/00,00.00	13/06,00.00
	14/08,00.00	10/00,00.00	11/20,00.00	17/00,00.00	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0
40.0	0/ 0. 0. 0	28/29,00.00	01/00,00.00	-1/-1,-1,-1	28/05,00.00	29/00,00.00	07/00,00.00	13/24,00.00
	08/00,00.00	10/18,00.00	20/11,00.00	17/00,00.00	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0
30.0	0/ 0. 0. 0	28/29,00.00	01/00,00.00	-1/-1,-1,-1	28/05,00.00	29/00,00.00	07/00,00.00	24/00,00.00
	08/00,00.00	18/10,00.00	20/00,00.00	17/00,00.00	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0	0/ 0. 0. 0



# APPENDIX C. SIXBIT LISTING

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PROGRAM SIXBIT
COMMON /A/      A(51)      ,ARK(4)      ,B(51)      ,SIXBIT
1 BRK(4)      ,CRK(4)      ,F(20)      ,FF(20)      ,SIXBIT
2 FLUX(120)    ,FLXINF(120) ,FRATE(20) ,FTERM(40) ,SIXBIT
3 FTERMW(40)   ,G(20)      ,GG(20)      ,HBR(20)      ,SIXBIT
4 H2HOLD(20)   ,H3HOLD(20) ,IATOM(10,20) ,IGAIN(4)      ,SIXBIT
5 IGA1NA(20,20) ,IGA1NB(20,20) ,IGA1NC(20,20) ,IGA1ND(20,20) ,SIXBIT
6 ILOSS(4)     ,ILOSSA(20,20) ,ILOSSB(20,20) ,ILOSSC(20,20) ,SIXBIT
7 ILOSSD(20,20) ,INFORM(30) ,JPULL(20) ,K(1000)      ,SIXBIT
8 K0(51)      ,KABS(20,120) ,KABS2(120) ,KABS02(120) ,SIXBIT
9 KABS03(120)  ,KRR(80)     ,L1(51)      ,L2(51)      ,SIXBIT
X L3(51)      ,LL1(21)     ,LL2(21)     ,LL3(21)     ,SIXBIT
1 N(51)      ,NASRAS(1000) ,NFTERM(20) ,NTERM(20) ,SIXBIT
2 NUSRUS(400) ,PHOLD(20,20) ,PROHLD(71,20) ,GOLD(20) ,SIXBIT
3 QRK(20)     ,R1(51)      ,R2(51)      ,R3(51)      ,SIXBIT
4 RR1(21)     ,RR2(21)     ,RR3(21)     ,SUMIN(10,20) ,SIXBIT
5 TABO2(87)   ,TABO3(87)   ,TEMP(20)    ,TERM(100)   ,SIXBIT
6 TERMW(100)  ,Y(20)      ,YHOLD(20,20) ,YLAST(20,20) ,SIXBIT
7 YNEW(20)    ,YOLD(20)    ,YPRINT(20,20) ,YSTART(20,20) ,SIXBIT
8 Y3SUN(20)   ,Y4SUN(20)   ,Z(20)      ,ZPRINT(20) ,SIXBIT
COMMON /B/     ALPHA , EQUIL , H , HCOUNT , IFLAG1 , IFLAG2 ,
2 IFLAG3 , IFLAG4 , IFLAG5 , IFLAG6 , IFLAG7 , IFLAG8 ,
3 IFLAG9 , IJ2X , ITCHXX , IUNIT , JCNTRL , JFLAG2 ,
4 JFLAG6 , JOSHUA , JZEND , JZMAIN , LAT , LONG ,
5 NFREAC , NREAC , NSPEC , P1 , T , TDAY ,
6 THOUR , TMAX1 , TMAX2 , TMIN , TMONTH , TOLD ,
7 TPRINT , TQUIT , TSEC , ZBOTUM , ZSTEP , ZTOP ,
INTEGER HCOUNT,PHOLD,R1,R2,R3,RR1,RR2,RR3,RX1,RX2,RX3,
1 TMONTH,TDAY,THOUR,TMIN,TSEC,TX
REAL K0,N,KABS,K,KRR,LAT,LONG,K5,K5MAX,KABS02,KABS03,KABS2
C DATA INPUT FORMATS, IN ORDER
C 1. JFLAG2 = 0 FOR FRESH START,
C = 1 FOR RESTART FROM TAPE.
C 2. JFLAG = 0 FOR NO MICROFILM,
C = 1 TO GET MICROFILM PLOTS.
C 3. THREE CARDS OF ALPHANUMERIC INFORMATION TO YOURSELF TO BE
C PRINTED OUT AT THE FIRST OF THE OUTPUT.
C 4. NORMAL REACTIONS WITH RATE COEFFICIENTS, READ IN REACTS, EACH
C CARD CONTAINS L1,L2,L3,R1,R2,R3,K0,A,N,B, WHERE L1,L2,L3, ARE THE
C SPECIES NUMBERS ON THE LEFT SIDE OF THE REACTION, R1,R2,R3 ARE
C THE SPECIES NUMBERS ON THE RIGHT SIDE, AND THE RATE COEFFICIENT IS
C GIVEN BY K=K0 * (TEMP/A)**N * EXPF(B/TEMP).
C FORMAT (3(I2,1X),1X,3(I2,1X),6X,2(E8.2,2X),2(E9.2,2X))
C SAMPLE ( / IS EDGE OF CARD)
C /07 03 09 05 08 01 4.50E-08 3.00E+02 -1.50E+00 -9.37E+02
C THIS SET MUST BE TERMINATED WITH A CARD CONTAINING A 99 IN
C COLUMNS 1 AND 2.
C 5. PHOTOREACTIONS WITH CROSS-SECTIONS AS A FUNCTION OF WAVE-LENGTH,
C READ IN REACTS.
C FIRST CARD - LL1,LL2,LL3,RR1,RR2,RR3 - SPECIES NUMBERS AS ABOVE.
C SECOND CARD - LAMDAX,LAMDAY - 1ST AND LAST WAVELENGTH INTERVAL
C NUMBERS FOR WHICH REACTION CROSS-SECTIONS ARE GIVEN.
C THIRD AND FOLLOWING CARDS - KABS - THE REACTION CROSS-SECTIONS.
C FORMAT (3(I2,1X),1X,3(I2,1X))
C FORMAT (13,2X,13)
C FORMAT (7(E8.2,2X))
C SAMPLE
C /03 01 01 02 09 01
C /047 112
C /4.93E-23 4.92E-23 4.91E-23 4.90E-23
C THIS SET MUST BE TERMINATED WITH A 99.

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6. ALTITUDE INFORMATION, READ IN HEIGHTS. THIS CAN BE GIVEN EITHER AS THE TOP AND BOTTOM ALTITUDES AND THE STEP SIZE (WHICH ALLOWS ONLY CONSTANT SPACING), OR AS A LIST OF ALTITUDES (WHICH CAN BE ANY SPACING, BUT MUST BE IN ORDER WITH THE HIGHEST ALTITUDE FIRST) THE FIRST VALUE ON THE CARD IS IFLAG6. IF IFLAG6=0, THEN THE NEXT THREE VALUES ARE TAKEN TO BE THE TOP AND BOTTOM ALTITUDES AND THE STEP SIZE, ALL IN KILOMETERS. IF IFLAG6 IS NOT ZERO, IT GIVES THE NUMBER OF ALTITUDE VALUES (IN KILOMETERS) WHICH FOLLOW. ZERO OR NEGATIVE VALUES OF ALTITUDES ARE NOT ALLOWED.  
 FORMAT (I2,6(2X,E9.3)) - FIRST CARD  
 FORMAT (6(E9.3,2X)) - ALL OTHER CARDS  
 SAMPLE NO. 1 (CONSTANT STEP SIZE)  
 /00 1.000E+02 3.000E+01 1.000E+01  
 SAMPLE NO. 2 (VARIABLE STEP SIZE)  
 /04 1.000E+02 9.500E+01 9.000E+01 8.000E+01

7. TEMPERATURE PROFILE, READ IN ALGEBRA.  
 FORMAT (7(E8.2,2X))  
 SAMPLE  
 /1.23E+02 1.37E+02 1.46E+02 1.70E+02

8. THE NUMBER OF ATOMS OF EACH DIFFERENT KIND PER MOLECULE. ON EACH CARD IS THE SPECIES NUMBER, THE NUMBER OF ATOMS OF THE FIRST KIND PER MOLECULE, THE NUMBER OF ATOMS OF THE SECOND KIND PER MOLECULE, ETC., OUT TO A MAXIMUM OF TEN KINDS OF ATOMS. THE KINDS OF ATOMS CAN BE ANYTHING, SUCH AS H ATOMS, NUMBER OF UNBALANCED ELECTRONS, ETC., BUT SHOULD BE ORDERED WITH LEAST NUMEROUS KIND FIRST OUT TO MOST NUMEROUS KIND (WHICH WILL NORMALLY BE THE TOTAL NUMBER OF ATOMS) LAST.  
 FORMAT (I2,2X,10(I1,1X))  
 SAMPLE  
 /07 2 1 0 0 1 0 4

9. FLAGS AND STARTING VALUES, READ IN START. INPUTS ARE  
 T - THE STARTING RUNNING TIME IN SECONDS (NORMALLY ZERO EXCEPT WHEN A RUN IS BEING RESTARTED)  
 TPRINT - THE DESIRED INTERVAL, IN SECONDS, BETWEEN PRINT-OUTS. THIS WILL AUTOMATICALLY INCREASE LATER IF THE STEPS GET BIG ENOUGH. 1 SECOND IS A REASONABLE CHOICE HERE.  
 TMAX1 - THE MAXIMUM VALUE WHICH TPRINT IS ALLOWED TO HAVE WHEN THE ATMOSPHERE IS IN FULL DAYLIGHT OR FULL DARKNESS. RECOMMENDED VALUE IS 3600 SECONDS.  
 TMAX2 - THE MAXIMUM VALUE WHICH TPRINT CAN HAVE DURING TWILIGHT. RECOMMENDED VALUE IS 60 SECONDS.  
 TQUIT - IF T REACHES THIS VALUE, THE PROGRAM STOPS (IN SECONDS).  
 IFLAG8 - =0 TO USE A RUNGE-KUTTA SOLUTION (RUNKUT)  
 =1 TO USE A PARTIAL INTEGRATION SOLUTION (WEIRD)  
 IFLAG1 - =1 LETS SPECIES GO INTO EQUILIBRIUM.  
 =0 DOESNT LET THEM.  
 EQUIL - THE VALUE OF THE FRACTIONAL CHANGE PER SECOND WHICH DEFINES EQUILIBRIUM. 1.0E-8 IS REASONABLE.  
 JOSHUA =0 GIVES NORMAL OPERATION.  
 =1 HOLDS THE ZENITH ANGLE AT ITS STARTING VALUE, USEFUL FOR DETERMINING STEADY-STATE VALUES.  
 FORMAT (5(E8.2,2X),2(I1,2X),E8.2,2X,I1)  
 SAMPLE  
 /0.00E+00 1.00E+00 3.60E+03 6.00E+01 8.64E+05 0 1 1.00E-08 0

10. LOCATION INFORMATION, READ IN ZENANG.  
 LAT = LATITUDE IN DEGREES

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C LONG = LONGITUDE IN DEGREES SIXBIT
C TMONTH = MONTH NUMBER (INTEGER) SIXBIT
C TDAY = DAY OF THE MONTH (INTEGER) SIXBIT
C THOUR = HOUR OF THE DAY (INTEGER) SIXBIT
C TMIN = MINUTE OF THE HOUR (INTEGER) SIXBIT
C TSEC = SECOND OF THE MINUTE (INTEGER) SIXBIT
C FORMAT (2(E9.2,2X),5(12,2X)) SIXBIT
C SAMPLE SIXBIT
C /+3.72E+01 +9.25E+01 03 05 23 00 00 SIXBIT
C SIXBIT
C 11. SPECIES NUMBER AND BEGINNING ALTITUDE PROFILE, READ IN START. SIXBIT
C PROFILE IS TAKEN TO BE ALL ZEROS IF NO PROFILE IS GIVEN. SIXBIT
C FORMAT (12) - FIRST CARD - SPECIES NUMBER SIXBIT
C FORMAT (7(E8.2,2X)) - FOLLOWING CARDS - ALTITUDE PROFILE SIXBIT
C SAMPLE SIXBIT
C /04 SIXBIT
C /9.37E+08 4.25E+09 8.34E+09 SIXBIT
C SIXBIT
C FLAG USAGE * * * * * SIXBIT
C IFLAG1 =1 LETS SPECIES GO INTO EQUILIBRIUM SIXBIT
C =0 DOESNT LET THEM. INPUT, SEE NO. 7. SIXBIT
C IFLAG2 - USED BY RUNKUT AND WIERD TO KNOW WHEN ITS TIME TO RETURN. SIXBIT
C IFLAG3 - USED BY ZENANG TO KNOW IF ITS THE FIRST TIME THROUGH. SIXBIT
C IFLAG4 AND IFLAG5 - USED BY SIXBIT TO INCREASE TPRINT. SEE NO. 7. SIXBIT
C IFLAG6 - USED BY START TO TELL IF AN O2 PROFILE HAS BEEN INPUT. SIXBIT
C IFLAG7 - USED TO TELL IF AN O3 PROFILE HAS BEEN INPUT. SIXBIT
C IFLAG8 - =0 TO USE RUNKUT SIXBIT
C =1 TO USE WEIRD. INPUT, SEE NO. 7. SIXBIT
C IFLAG9 - USED BY MOST SUBROUTINES TO FIND INPUT ERRORS AND SIXBIT
C TERMINATE THE RUN. SIXBIT
C JOSHUA = 0 LETS THE SUN MOVE NATURALLY, SIXBIT
C = 1 HOLDS THE SUN FIXED IN THE SKY. (INPUT) SIXBIT
C JFLAG2 = 0 FOR FRESH START, SIXBIT
C = 1 FOR RESTART (INPUT). SIXBIT
C JFLAG6 = 0 IF ALTITUDES ARE GIVEN AS TOP, BOTTOM, AND STEP SIZE, SIXBIT
C = THE NUMBER OF ALTITUDES IF GIVEN IN TABULAR FORM. (INPUT) SIXBIT
C JJFLAG = 0 FOR NO MICROFILM, SIXBIT
C = 1 TO GET MICROFILM PLOTS OF THE PROFILES. (INPUT) SIXBIT
C READ (13,997) IUNIT SIXBIT
C REWIND 13 SIXBIT
C READ (60,997) JLAG2 SIXBIT
C READ (60,997) JJFLAG SIXBIT
C IUNIT = 60 SIXBIT
C IF (JFLAG2 .EQ. 1) IUNIT = 13 SIXBIT
C READ (60,996) (INFORM(INFO),INFO=1,30) SIXBIT
C PRINT 995, (INFORM(INFO),INFO=1,30) SIXBIT
C IFLAG9=0 SIXBIT
C CALL REACTS SIXBIT
C IF (IFLAG9 .EQ. 1) GO TO 9000 SIXBIT
C CALL HEIGHTS SIXBIT
C IF (IFLAG9 .EQ. 1) GO TO 9000 SIXBIT
C CALL ALGEBRA SIXBIT
C IF (IFLAG9 .EQ. 1) GO TO 9000 SIXBIT
C CALL START SIXBIT
C IF (IFLAG9 .EQ. 1) GO TO 9000 SIXBIT
10 CALL ZENANG SIXBIT
C IF (IFLAG9 .EQ. 1) GO TO 9000 SIXBIT
C DO 100 JZMAIN = ,JZEND SIXBIT
C JJZX = JZEND-JZ IN SIXBIT
C DO 30 M1=1,NSPE SIXBIT

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      Y(M1) = YHOLD(M1,JZMAIN)                                SIXBIT
30  CONTINUE                                                    SIXBIT
      CALL PRODUC                                              SIXBIT
      HCOUNT = 0                                             SIXBIT
      IF (IFLAG8 .EQ. 1) GO TO 40                             SIXBIT
      CALL RUNKUT                                             SIXBIT
      GO TO 50                                                SIXBIT
40  CALL WEIRD                                                SIXBIT
50  HBAR(JZMAIN) = TPRINT/HCOUNT                               SIXBIT
      IFLAG2 = 0                                             SIXBIT
      DO 65 ITC=1,ITCXX                                       SIXBIT
      SUM = 0.0                                              SIXBIT
      DO 55 M2=3,NSPEC                                       SIXBIT
      SUM = SUM + Y(M2)*IATOM(ITC,M2)                       SIXBIT
55  CONTINUE                                                    SIXBIT
      IF (SUM .LT. 1.0) GO TO 65                             SIXBIT
      DO 60 M22 = 3,NSPEC                                       SIXBIT
      IF (IATOM(ITC,M22) .EQ. 0) GO TO 60                     SIXBIT
      Y(M22) = Y(M22)*SUMIN(ITC,JZMAIN)/SUM                  SIXBIT
60  CONTINUE                                                    SIXBIT
      Y(2) = Y(2)*SUMIN(ITC,JZMAIN)/SUM                      SIXBIT
65  CONTINUE                                                    SIXBIT
      DO 70 M222=2,NSPEC                                       SIXBIT
      YHOLD(M222,JZMAIN) = Y(M222)                          SIXBIT
70  CONTINUE                                                    SIXBIT
      DO 73 I=1,NREAC                                         SIXBIT
      PROHLD(I,JZMAIN) = TERM(I)                             SIXBIT
73  CONTINUE                                                    SIXBIT
      DO 76 II=1,NFREAC                                        SIXBIT
      PROHLD(II+NREAC,JZMAIN) = FTERM(II)                   SIXBIT
76  CONTINUE                                                    SIXBIT
      T = TOLD                                                SIXBIT
100 CONTINUE                                                    SIXBIT
      T = T + TPRINT                                           SIXBIT
      IF (IFLAG1 .EQ. 0) GO TO 150                             SIXBIT
C  FIND OUT WHAT HAS GONE INTO EQUILIBRIUM                     SIXBIT
      DO 140 JZ1=1,JZEND                                       SIXBIT
      IF (JPULL(JZ1) .EQ. 1) GO TO 140                         SIXBIT
      PCHECK = 0                                             SIXBIT
      DO 130 M4=3,NSPEC                                       SIXBIT
      PHOLD(M4,JZ1) = 0                                       SIXBIT
      IF (YHOLD(M4,JZ1) .LT. 1.0E-50 .AND. YLAST (M4,JZ1) .LT. 1.0E-50) SIXBIT
      GO TO 110                                                SIXBIT
      IF (YLAST(M4,JZ1) .LT. 1.0E-50) GO TO 130               SIXBIT
      IF (ABS(1.0-YHOLD(M4,JZ1)/YLAST(M4,JZ1)) .LT. EQUIL*TPRINT) SIXBIT
      GO TO 110                                                SIXBIT
      GO TO 130                                                SIXBIT
110 PHOLD(M4,JZ1) = 1                                           SIXBIT
120 PCHECK = PCHECK+1                                           SIXBIT
130 CONTINUE                                                    SIXBIT
      IF (PCHECK+2 .LT. NSPEC) GO TO 140                     SIXBIT
      JPULL(JZ1) = 1                                           SIXBIT
      HBAR(JZ1) = TQUIT                                       SIXBIT
140 CONTINUE                                                    SIXBIT
C  SET UP AND PRINT OUT ALL THE SPECIES                         SIXBIT
150 DO 170 JZ2=1,JZEND                                       SIXBIT
      ZPRINT(JZ2) = Z(JZ2)*(1.0-2.0*JPULL(JZ2))             SIXBIT
      YPRINT(2,JZ2) = YHOLD(2,JZ2)                           SIXBIT
      DO 160 M5=3,NSPEC                                       SIXBIT
      YPRINT(M5,JZ2) = YHOLD(M5,JZ2)*(1.0-2.0*PHOLD(M5,JZ2)) SIXBIT

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160	CONTINUE	SIXBIT
170	CONTINUE	SIXBIT
	CALL PHYSICS	SIXBIT
	CALL HANDLE	SIXBIT
	IF (JJFLAG .NE. 1) GO TO 175	SIXBIT
	CALL MICROPLT	SIXBIT
175	TOLD = T	SIXBIT
	IF (TOLD .GE. TQUIT) GO TO 800	SIXBIT
C	ADJUST TPRINT IF NECESSARY	SIXBIT
	IFLAG4 = IFLAG4+1	SIXBIT
	IF (IFLAG4 .LT. 10) GO TO 188	SIXBIT
	IFLAG4 = 0	SIXBIT
	IFLAG5 = IFLAG5+1	SIXBIT
	IF (IFLAG5 .GT. 9) IFLAG5 = 0	SIXBIT
	HMIN = TPRINT	SIXBIT
	DO 180 JZ3=1,JZEND	SIXBIT
	IF (HBAR(JZ3) .LT. HMIN) HMIN = HBAR(JZ3)	SIXBIT
180	CONTINUE	SIXBIT
	IF (HMIN/TPRINT .LT. 0.001) GO TO 188	SIXBIT
	IF (ALPHA .LT. 90.0 .OR. ALPHA .GT. 90.0+SQRTF(Z(1))) GO TO 182	SIXBIT
	IF (TPRINT*10.0 .LT. TMAX2) GO TO 184	SIXBIT
	TPRINT = TMAX2	SIXBIT
	GO TO 190	SIXBIT
182	IF (TPRINT*10.0 .LT. TMAX1) GO TO 184	SIXBIT
	TPRINT = TMAX1	SIXBIT
	GO TO 190	SIXBIT
184	TPRINT = TPRINT*10.0	SIXBIT
	IFLAG4 = IFLAG5	SIXBIT
	IFLAG5 = 0	SIXBIT
	GO TO 190	SIXBIT
188	IF (ALPHA .GT. 90.0 .AND. ALPHA .LT. 90.0+SQRTF(Z(1)))	SIXBIT
1	.AND. TPRINT .GT. TMAX2) TPRINT = TMAX2	SIXBIT
190	DO 210 JZ4=1,JZEND	SIXBIT
	DO 200 M6=3,NSPEC	SIXBIT
	YLAST(M6,JZ4) = YHOLD(M6,JZ4)	SIXBIT
200	CONTINUE	SIXBIT
210	CONTINUE	SIXBIT
	DO 220 JZ5=1,JZEND	SIXBIT
	IF (JPULL(JZ5) .EQ. 0) GO TO 10	SIXBIT
220	CONTINUE	SIXBIT
700	PRINT 999	SIXBIT
	GO TO 9000	SIXBIT
800	PRINT 998	SIXBIT
995	FORMAT(1H0,10A8)	SIXBIT
996	FORMAT(10A8)	SIXBIT
997	FORMAT(11)	SIXBIT
998	FORMAT(1H0,*THE RUNNING TIME HAS REACHED TQUIT, THE QUITTING TIME	SIXBIT
1	THAT WAS INPUT IN SUBROUTINE START.*)	SIXBIT
999	FORMAT(1H0,*ALL SPECIES AT ALL ALTITUDES ARE NOW IN EQUILIBRIUM.*)	SIXBIT
9000	END	SIXBIT-

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SUBROUTINE REACTS
COMMON /A/ A(51) ,ARK(4) ,B(51) , REACTS
1 BRK(4) ,CRK(4) ,F(20) ,FF(20) , REACTS
2 FLUX(120) ,FLXINF(120) ,FRATE(20) ,FTERM(40) , REACTS
3 FTERMW(40) ,G(20) ,GG(20) ,HBAR(20) , REACTS
4 H2HOLD(20) ,H3HOLD(20) ,IATOM(10,20) ,IGAIN(4) , REACTS
5 IGAINA(20,20) ,IGAINB(20,20) ,IGAINC(20,20) ,IGAIND(20,20) , REACTS
6 ILOSS(4) ,ILOSSA(20,20) ,ILOSSB(20,20) ,ILOSSC(20,20) , REACTS
7 ILOSSD(20,20) ,INFORM(30) ,JPULL(20) ,K(1000) , REACTS
8 K0(51) ,KABS(20,120) ,KABSN2(120) ,KABSO2(120) , REACTS
9 KABSO3(120) ,KPK(80) ,L1(51) ,L2(51) , REACTS
X L3(51) ,LL1(21) ,LL2(21) ,LL3(21) , REACTS
1 N(51) ,NASRAS(1000) ,NFTERM(20) ,NTERM(20) , REACTS
2 NUSRUS(400) ,PHOLD(20,20) ,PROHLD(71,20) ,QOLD(20) , REACTS
3 ORK(20) ,R1(51) ,R2(51) ,R3(51) , REACTS
4 RR1(21) ,RR2(21) ,RR3(21) ,SUMIN(10,20) , REACTS
5 TABO2(87) ,TABO3(87) ,TEMP(20) ,TERM(100) , REACTS
6 TERMW(100) ,Y(20) ,YHOLD(20,20) ,YLAST(20,20) , REACTS
7 YNEW(20) ,YOLD(20) ,YPRINT(20,20) ,YSTART(20,20) , REACTS
8 Y3SUN(20) ,Y4SUN(20) ,Z(20) ,ZPRINT(20) , REACTS
COMMON /B/ ALPHA ,EQUIL , H , HCOUNT , IFLAG1 , IFLAG2 , REACTS
2 IFLAG3 , IFLAG4 , IFLAG5 , IFLAG6 , IFLAG7 , IFLAG8 , REACTS
3 IFLAG9 , IJZX , ITCHXX , IUNIT , JCNTRL , JFLAG2 , REACTS
4 JFLAG6 , JOSHUA , JZEND , JZMAIN , LAT , LONG , REACTS
5 NFREAC , NREAC , NSPEC , PI , T , TDAY , REACTS
6 THOUR , TMAX1 , TMAX2 , TMIN , TMONTH , TOLD , REACTS
7 TPRINT , TQUIT , TSEC , ZBOTUM , ZSTEP , ZTOP , REACTS
INTEGER HCOUNT,PHOLD,R1,R2,R3,RR1,RR2,RR3,RX1,RX2,RX3, REACTS
1 TMONTH,TDAY,THOUR,TMIN,TSEC,TX REACTS
REAL KO,N,KABS,K,KRK,LAT,LONG,K5,K5MAX,KABSO2,KABSO3,KABSN2 REACTS
NSPEC = 0 REACTS
DO 10 I1=1,51 REACTS
READ (60 ,999) L1(I1),L2(I1),L3(I1),R1(I1),R2(I1),R3(I1), REACTS
1 KO(I1),A(I1),N(I1),B(I1) REACTS
IF (L1(I1) .EQ. 99) GO TO 20 REACTS
IXX =XMAXOF(L1(I1),L2(I1),L3(I1),R1(I1),R2(I1),R3(I1)) REACTS
IF (IXX .GT. NSPEC) NSPEC = IXX REACTS
10 CONTINUE REACTS
PRINT 998 REACTS
IFLAG9 = 1 REACTS
GO TO 900 REACTS
20 NREAC = I1-1 REACTS
NSPEC = NSPEC+2 REACTS
PRINT 997,NREAC,NSPEC REACTS
PRINT 991 , (I3,L1(I3),L2(I3),L3(I3),R1(I3),R2(I3),R3(I3), REACTS
1 KO(I3),A(I3),N(I3),B(I3),I3=1,NREAC) REACTS
NSPEC = NSPEC+2 REACTS
DO 30 I2=1,21 REACTS
READ (60 ,996) LL1(I2),LL2(I2),LL3(I2),RR1(I2),RR2(I2),RR3(I2) REACTS
IF (LL1(I2) .EQ. 99) GO TO 40 REACTS
READ (60,992) LAMDA1,LAMDA2 REACTS
READ (60 ,995) (KABS(I2,LAMDA),LAMDA=LAMDA1,LAMDA2) REACTS
30 CONTINUE REACTS
PRINT 994 REACTS

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      IFLAG9 = 1                      REACTS
      GO TO 900                      REACTS
40    NFREAC = I2-1                  REACTS
      PRINT 993,NFREAC                REACTS
      DO 50 I5 = 1,NFREAC            REACTS
      I4 = I5+NFREAC                  REACTS
      PRINT 990, I4,LL1(I5),RR1(I5),RR2(I5),RR3(I5) REACTS
50    CONTINUE                       REACTS
999  FORMAT(3(I2,1X),1X,3(I2,1X),6X,2(E8.2,2X),2(E9.2,2X)) REACTS
998  FORMAT(1H ,*NO END CARD FOUND WHEN READING THE REACTION SET IN SUBREACTS
1ROUTINE REACTS.*,/*THIS WILL TERMINATE THE RUN. SORRY.*) REACTS
997  FORMAT(1H ,*THERE HAVE BEEN *,I2,* REACTIONS INPUT INVOLVING *,I2,REACTS
1* SPECIES.*,/1X*THE REACTIONS AND THEIR RATE COEFFICIENTS ARE */,)REACTS
996  FORMAT (3(I2,1X),1X,3(I2,1X)) REACTS
995  FORMAT(7(E8.2,2X)) REACTS
994  FORMAT(1H ,*NO END CARD FOUND WHEN READING THE PHOTOREACTIONS IN SREACTS
1UBROUTINE REACTS.*,/*THIS WILL TERMINATE THE RUN. TOUGH LUCK.*) REACTS
993  FORMAT(1H0,*THERE HAVE BEEN *,I2,* PHOTOREACTIONS INPUT.*) REACTS
992  FORMAT(I3,2X,I3) REACTS
991  FORMAT(1H ,I2,3X,2(I2,**),I2,---*,2(I2,**),I2,* K = *,E8.2, REACTS
17H*(TEMP/,E8.2,3H)**F5.2,6H*EXPF(,E9.2,*/TEMP)*,///) REACTS
990  FORMAT (1H ,I2,4X,I2,** PHOTON ---*,2(I2,**),I2,///) REACTS
900  RETURN                          REACTS
      END                            REACTS-

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SUBROUTINE HEIGHTS
COMMON /A/ A(51) ,ARK(4) ,B(51) ,HEIGHTS
1 BRK(4) ,CRK(4) ,F(20) ,FF(20) ,HEIGHTS
2 FLUX(120) ,FLXINF(120) ,FRATE(20) ,FTERM(40) ,HEIGHTS
3 FTERMW(40) ,G(20) ,GG(20) ,HBAR(20) ,HEIGHTS
4 H2HOLD(20) ,H3HOLD(20) ,IATOM(10,20) ,IGAIN(4) ,HEIGHTS
5 IGAINA(20,20) ,IGAINB(20,20) ,IGAINC(20,20) ,IGAIND(20,20) ,HEIGHTS
6 ILOSS(4) ,ILOSSA(20,20) ,ILOSSB(20,20) ,ILOSSC(20,20) ,HEIGHTS
7 ILOSSD(20,20) ,INFORM(30) ,JPULL(20) ,K(1000) ,HEIGHTS
8 K0(51) ,KABS(20,120) ,KABS2(120) ,KABS02(120) ,HEIGHTS
9 KABS03(120) ,KRK(80) ,L1(51) ,L2(51) ,HEIGHTS
X L3(51) ,LL1(21) ,LL2(21) ,LL3(21) ,HEIGHTS
1 N(51) ,NASRAS(1000) ,NFTERM(20) ,NTERM(20) ,HEIGHTS
2 NUSRUS(400) ,PHOLD(20,20) ,PROHLD(71,20) ,QOLD(20) ,HEIGHTS
3 QRK(20) ,R1(51) ,R2(51) ,R3(51) ,HEIGHTS
4 RR1(21) ,RR2(21) ,RR3(21) ,SUMIN(10,20) ,HEIGHTS
5 TABO2(87) ,TABO3(87) ,TEMP(20) ,TERM(100) ,HEIGHTS
6 TERMW(100) ,Y(20) ,YHOLD(20,20) ,YLAST(20,20) ,HEIGHTS
7 YNEW(20) ,YOLD(20) ,YPRINT(20,20) ,YSTART(20,20) ,HEIGHTS
8 Y3SUN(20) ,Y4SUN(20) ,Z(20) ,ZPRINT(20) ,HEIGHTS
COMMON /B/ ALPHA, EQUIL, H , HCOUNT, IFLAG1, IFLAG2, HEIGHTS
2 IFLAG3, IFLAG4, IFLAG5, IFLAG6, IFLAG7, IFLAG8, HEIGHTS
3 IFLAG9, IJZX, ITCHXX, IUNIT, JCNTRL, JFLAG2, HEIGHTS
4 JFLAG6, JOSHUA, JZEND, JZMAIN, LAT , LONG , HEIGHTS
5 NFREAC, NREAC, NSPEC, PI , T , TDAY , HEIGHTS
6 THOUR , TMAX1, TMAX2, TMIN , TMONTH, TOLD , HEIGHTS
7 TPRINT, TQUIT, TSEC , ZBOTUM, ZSTEP , ZTOP , HEIGHTS
INTEGER HCOUNT, PHOLD, R1, R2, R3, RR1, RR2, RR3, RX1, RX2, RX3, HEIGHTS
1 TMONTH, TDAY, THOUR, TMIN, TSEC, TX , HEIGHTS
REAL K0, N, KABS, K, KRK, LAT, LONG, K5, K5MAX, KABS02, KABS03, KABS2 , HEIGHTS
READ (60 , 999) JFLAG6, (Z(JZ1), JZ1=1,6) , HEIGHTS
IF (JFLAG6 .EQ. 0) GO TO 100 , HEIGHTS
JZEND = JFLAG6 , HEIGHTS
IF (JZEND .LT. 7) GO TO 200 , HEIGHTS
READ (60,997) (Z(JZ2), JZ2=7, JZEND) , HEIGHTS
GO TO 200 , HEIGHTS
100 ZTOP = Z(1) , HEIGHTS
ZBOTUM = Z(2) , HEIGHTS
ZSTEP = Z(3) , HEIGHTS
JZEND = (ZTOP-ZBOTUM)/ZSTEP + 1 , HEIGHTS
DO 110 JZ3=1, JZEND , HEIGHTS
Z(JZ3) = ZTOP - (JZ3-1)*ZSTEP , HEIGHTS
110 CONTINUE , HEIGHTS
IF (Z(JZEND) .EQ. ZBOTUM) GO TO 200 , HEIGHTS
PRINT 998 , HEIGHTS
IFLAG9 = 1 , HEIGHTS
GO TO 9000 , HEIGHTS
200 DO 210 JZ4=1, JZEND , HEIGHTS
ZPRINT(JZ4) = Z(JZ4) , HEIGHTS
210 CONTINUE , HEIGHTS
997 FORMAT(6(E9.3, 2X)) , HEIGHTS
998 FORMAT(1H0, *ALTITUDES DONT CHECK OUT IN SUBROUTINE HEIGHTS. THIS W , HEIGHTS
11LL TERMINATE THE RUN.*) , HEIGHTS
999 FORMAT(I2, 6(2X, E9.3)) , HEIGHTS
9000 RETURN , HEIGHTS
END , HEIGHT-

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SUBROUTINE ALGEBRA
COMMON /A/
1 BRK(4) , A(51) , ARK(4) , B(51) , ALGEBRA
2 FLUX(120) , CRK(4) , F(20) , FF(20) , ALGEBRA
3 FTERMW(40) , FLXINF(120) , FRATE(20) , FTERM(40) , ALGEBRA
4 H2HOLD(20) , G(20) , GG(20) , HBAR(20) , ALGEBRA
5 IGA1NA(20,20) , H3HOLD(20) , IATOM(10,20) , IGA1N(4) , ALGEBRA
6 ILOSS(4) , IGA1NB(20,20) , IGA1NC(20,20) , IGA1ND(20,20) , ALGEBRA
7 ILOSSD(20,20) , ILOSSA(20,20) , ILOSSB(20,20) , ILOSSC(20,20) , ALGEBRA
8 K0(51) , INFORM(30) , JPULL(20) , K(1000) , ALGEBRA
9 KABS03(120) , KABS(20,120) , KABS2(120) , KABS02(120) , ALGEBRA
X L3(51) , KRK(80) , L1(51) , L2(51) , ALGEBRA
1 N(51) , LL1(21) , LL2(21) , LL3(21) , ALGEBRA
2 NUSRUS(400) , NASRAS(1000) , NFTERM(20) , NTERM(20) , ALGEBRA
3 ORK(20) , PHOLD(20,20) , PROHLD(71,20) , QOLD(20) , ALGEBRA
4 RRI(21) , R1(51) , R2(51) , R3(51) , ALGEBRA
5 TABO2(87) , RR2(21) , RR3(21) , SUMIN(10,20) , ALGEBRA
6 TERMW(100) , TABO3(87) , TEMP(20) , TERM(100) , ALGEBRA
7 YNEW(20) , Y(20) , YHOLD(20,20) , YLAST(20,20) , ALGEBRA
8 Y3SUN(20) , YOLD(20) , YPRINT(20,20) , YSTART(20,20) , ALGEBRA
COMMON /B/ ALPHA , EQUIL , H , HCOUNT , IFLAG1 , IFLAG2 , ALGEBRA
2 IFLAG3 , IFLAG4 , IFLAG5 , IFLAG6 , IFLAG7 , IFLAG8 , ALGEBRA
3 IFLAG9 , IJZX , ITCHXX , IUNIT , JCNTRL , JFLAG2 , ALGEBRA
4 JFLAG6 , JOSHUA , JZEND , JZMAIN , LAT , LONG , ALGEBRA
5 NFREAC , NREAC , NSPEC , PI , T , TDAY , ALGEBRA
6 THOUR , TMAX1 , TMAX2 , TMIN , TMONTH , TOLD , ALGEBRA
7 TPRINT , TQUIT , TSEC , ZBOTUM , ZSTEP , ZTOP , ALGEBRA
INTEGER HCOUNT,PHOLD,R1,R2,R3,RR1,RR2,RR3,RX1,RX2,RX3, ALGEBRA
1 TMONTH,TDAY,THOUR,TMIN,TSEC,TX ALGEBRA
REAL K0,N,KABS,K,KRK,LAT,LONG,K5,K5MAX,KABS02,KABS03,KABS2 ALGEBRA
READ (60 ,999) (TEMP(JZ1),JZ1=1,JZEND) ALGEBRA
DO 10 I1=1,NREAC ALGEBRA
IXX = (I1-1)*JZEND ALGEBRA
DO 10 JZ2=1,JZEND ALGEBRA
IJZ = IXX + JZ2 ALGEBRA
K(IJZ) = K0(I1)*(TEMP(JZ2)/A(I1))*N(I1)*EXP(B(I1)/TEMP(JZ2)) ALGEBRA
PROHLD(I1,JZ2) = K(IJZ) ALGEBRA
10 CONTINUE ALGEBRA
DO 20 M1=1,NSPEC ALGEBRA
NTERM(M1) = 0 ALGEBRA
20 CONTINUE ALGEBRA
DO 30 IZERO = 1,1000 ALGEBRA
NASRAS(IZERO) = 0 ALGEBRA
30 CONTINUE ALGEBRA
DO 260 I2=1,NREAC ALGEBRA
LX1 = L1(I2) ALGEBRA
LX2 = L2(I2) ALGEBRA
LX3 = L3(I2) ALGEBRA
RX1 = R1(I2) ALGEBRA
RX2 = R2(I2) ALGEBRA
RX3 = R3(I2) ALGEBRA
IF (LX1.LT. 3) GO TO 130 ALGEBRA
IF (RX1.NE. LX1) GO TO 130 ALGEBRA
LX1= 1 ALGEBRA

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	RX1 = 1	ALGEBRA
	GO TO 130	ALGEBRA
110	IF (RX2 .NE. LX1) GO TO 120	ALGEBRA
	LX1 = 1	ALGEBRA
	RX2 = 1	ALGEBRA
	GO TO 130	ALGEBRA
120	IF (RX3 .NE. LX1) GO TO 130	ALGEBRA
	LX1 = 1	ALGEBRA
	RX3 = 1	ALGEBRA
130	IF (LX2 .LT. 3) GO TO 160	ALGEBRA
	IF (RX1 .NE. LX2) GO TO 140	ALGEBRA
	LX2 = 1	ALGEBRA
	RX1 = 1	ALGEBRA
	GO TO 160	ALGEBRA
140	IF (RX2 .NE. LX2) GO TO 150	ALGEBRA
	LX2 = 1	ALGEBRA
	RX2 = 1	ALGEBRA
	GO TO 160	ALGEBRA
150	IF (RX3 .NE. LX2) GO TO 160	ALGEBRA
	LX2 = 1	ALGEBRA
	RX3 = 1	ALGEBRA
160	IF (LX3 .LT. 3) GO TO 200	ALGEBRA
	IF (RX1 .NE. LX3) GO TO 170	ALGEBRA
	LX3 = 1	ALGEBRA
	RX1 = 1	ALGEBRA
	GO TO 200	ALGEBRA
170	IF (RX2 .NE. LX3) GO TO 180	ALGEBRA
	LX3 = 1	ALGEBRA
	RX2 = 1	ALGEBRA
	GO TO 200	ALGEBRA
180	IF (RX3 .NE. LX3) GO TO 200	ALGEBRA
	LX3 = 1	ALGEBRA
	RX3 = 1	ALGEBRA
200	IF (LX1 .LT. 3) GO TO 210	ALGEBRA
	NTERM(LX1) = NTERM(LX1)+1	ALGEBRA
	NASRAS((LX1-3)*NREAC+NTERM(LX1)) = 12	ALGEBRA
210	IF (LX2 .LT. 3) GO TO 220	ALGEBRA
	NTERM(LX2) = NTERM(LX2)+1	ALGEBRA
	NASRAS((LX2-3)*NREAC+NTERM(LX2)) = 12	ALGEBRA
220	IF (LX3 .LT. 3) GO TO 230	ALGEBRA
	NTERM(LX3) = NTERM(LX3)+1	ALGEBRA
	NASRAS((LX3-3)*NREAC+NTERM(LX3)) = 12	ALGEBRA
230	IF (RX1 .LT. 3) GO TO 240	ALGEBRA
	NTERM(RX1) = NTERM(RX1)+1	ALGEBRA
	NASRAS((RX1-3)*NREAC+NTERM(RX1)) = 12+NREAC	ALGEBRA
240	IF (RX2 .LT. 3) GO TO 250	ALGEBRA
	NTERM(RX2) = NTERM(RX2)+1	ALGEBRA
	NASRAS((RX2-3)*NREAC+NTERM(RX2)) = 12+NREAC	ALGEBRA
250	IF (RX3 .LT. 3) GO TO 260	ALGEBRA
	NTERM(RX3) = NTERM(RX3)+1	ALGEBRA
	NASRAS((RX3-3)*NREAC+NTERM(RX3)) = 12+NREAC	ALGEBRA
260	CONTINUE	ALGEBRA
	DO 310 IZERO=1,400	ALGEBRA
	NUSRUS(IZERO) = 0	ALGEBRA

310	CONTINUE	ALGEBRA
	DO 320 M2=1,NSPEC	ALGEBRA
	NFTERM(M2)=0	ALGEBRA
320	CONTINUE	ALGEBRA
	DO 350 I11=1,NFREAC	ALGEBRA
	NFTERM(LL1(I11)) = NFTERM(LL1(I11)) + 1	ALGEBRA
	NUSRUS((LL1(I11)-3)*NFREAC+NFTERM(LL1(I11))) = I11	ALGEBRA
	IF (RR1(I11) .LT. 3) GO TO 330	ALGEBRA
	NFTERM(RR1(I11)) = NFTERM(RR1(I11)) + 1	ALGEBRA
	NUSRUS((RR1(I11)-3)*NFREAC+NFTERM(RR1(I11))) = I11+NFREAC	ALGEBRA
330	IF (RR2(I11) .LT. 3) GO TO 340	ALGEBRA
	NFTERM(RR2(I11)) = NFTERM(RR2(I11)) + 1	ALGEBRA
	NUSRUS((RR2(I11)-3)*NFREAC+NFTERM(RR2(I11))) = I11+NFREAC	ALGEBRA
340	IF (RR3(I11) .LT. 3) GO TO 350	ALGEBRA
	NFTERM(RR3(I11)) = NFTERM(RR3(I11)) + 1	ALGEBRA
	NUSRUS((RR3(I11)-3)*NFREAC+NFTERM(RR3(I11))) = I11+NFREAC	ALGEBRA
350	CONTINUE	ALGEBRA
999	FORMAT (7(E8.2,2X))	ALGEBRA
	RETURN	ALGEBRA
	END	ALGEBR-

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SUBROUTINE START
COMMON /A/      A(51)          ,ARK(4)          ,B(51)          , START
1 BRK(4)        ,CRK(4)          ,F(20)          ,FF(20)          , START
2 FLUX(120)     ,FLXINF(120)    ,FRATE(20)     ,FTERM(40)     , START
3 FTERMW(40)    ,G(20)          ,GG(20)         ,HBAR(20)     , START
4 H2HOLD(20)    ,H3HOLD(20)    ,IATOM(10,20)   ,IGAIN(4)     , START
5 IGA1NA(20,20),IGAINB(20,20)  ,IGAINC(20,20)  ,IGAIND(20,20) , START
6 ILOSS(4)      ,ILOSSA(20,20) ,ILOSSB(20,20) ,ILOSSC(20,20) , START
7 ILOSSD(20,20),INFORM(30)     ,JPULL(20)     ,K(1000)     , START
8 K0(51)        ,KABS(20,120)   ,KABS2(120)   ,KABS02(120)  , START
9 KABS03(120)   ,KRK(80)        ,L1(51)        ,L2(51)        , START
X L3(51)        ,LL1(21)       ,LL2(21)       ,LL3(21)       , START
1 N(51)         ,NASRAS(1000)  ,NFTERM(20)  ,NTERM(20)   , START
2 NUSRUS(400)  ,PHOLD(20,20)  ,PROHLD(71,20),OOLD(20)   , START
3 QRK(20)      ,R1(51)        ,R2(51)        ,R3(51)        , START
4 RR1(21)      ,RR2(21)       ,RR3(21)       ,SUMIN(10,20) , START
5 TAB02(87)    ,TAB03(87)     ,TEMP(20)      ,TERM(100)   , START
6 TERMW(100)   ,Y(20)        ,YHOLD(20,20)   ,YLAST(20,20) , START
7 YNEW(20)     ,YOLD(20)      ,YPRINT(20,20)  ,YSTART(20,20) , START
8 Y3SUN(20)    ,Y4SUN(20)     ,Z(20)        ,ZPRINT(20)   , START
COMMON /B/     ALPHA , EQUIL , H          , HCOUNT, IFLAG1, IFLAG2,
2 IFLAG3, IFLAG4, IFLAG5, IFLAG6, IFLAG7, IFLAG8, START
3 IFLAG9, IJZX , ITCHXX, IUNIT , JCNTRL, JFLAG2, START
4 JFLAG6, JOSHUA, JZEND , JZMAIN, LAT , LONG , START
5 NFREAC, NREAC , NSPEC , PI , T , TDAY , START
6 THOUR , TMAX1 , TMAX2 , TMIN , TMONTH, TOLD , START
7 TPRINT, TQUIT , TSEC , ZBOTUM, ZSTEP , ZTOP , START
INTEGER HCOUNT,PHOLD,R1,R2,R3,RR1,RR2,RR3,RX1,RX2,RX3, START
1 TMONTH,TDAY,THOUR,TMIN,TSEC,TX          , START
REAL K0,N,KABS,K,KRK,LAT,LONG,K5,K5MAX,KABS02,KABS03,KABS2, START
DATA (IFLAG2=0),(IFLAG3=0),(IFLAG6=0),(IFLAG7=0),(PI=3.141592654), START
1 ((ARK(I),I=1,4)=0.5,0.292893,1.707107,0.166666667), START
2 ((BRK(I),I=1,4)=2.0,1.0,1.0,2.0), START
3 ((CRK(I),I=1,4)=0.5,0.292893,1.707107,0.5), START
4 ((HBAR(JZ),JZ=1,20) = 20(1.0)), START
5 ((JPULL(JZ),JZ=1,20) = 20(0)), START
6 (((YHOLD(M,JZ),M=1,2),JZ=1,20) = 40(1.0)), START
7 (((YPRINT(M,JZ),M=1,2),JZ=1,20) = 40(1.0)), START
8 (((PHOLD(M,JZ),M=1,2),JZ=1,20) = 40(1)), START
9 (((YHOLD(M,JZ),M=3,20),JZ=1,20) = 360(0.0)), START
1 (((SUMIN(ITCH,JZ),ITCH=1,10),JZ=1,20) = 200(0)), START
2 (((PHOLD(M,JZ),M=3,20),JZ=1,20) = 360(0)) , START
DATA (FLXINF(LAMDA),LAMDA=1,60) =
1 3.79E08, 2.65E09, 3.80E09, 8.83E09, 3.52E09, 7.71E09, 5.08E09, START
2 5.88E09, 1.20E10, 2.16E10, 1.75E10, 1.03E10, 3.94E11, 2.72E10, START
3 7.30E10, 2.54E11, 1.03E12, 1.59E12, 3.74E12, 8.88E12, 1.64E13, START
4 3.58E13, 5.68E13, 7.10E13, 9.90E13, 1.45E14, 2.21E14, 3.12E14, START
5 6.12E14, 9.38E14, 1.09E15, 1.27E15, 1.49E15, 1.83E15, 2.05E15, START
6 2.12E15, 2.23E15, 2.40E15, 2.36E15, 3.06E15, 3.53E15, 3.93E15, START
7 4.25E15, 4.45E15, 4.73E15, 4.94E15, 5.00E15, 5.20E15, 5.20E15, START
8 5.20E15, 5.20E15, 5.20E15, 5.30E15, 5.30E15, 5.40E15, 5.40E15, START
9 5.40E15, 5.40E15, 5.40E15, 5.40E15, 5.40E15, START
DATA ((FLXINF(LAMDA),LAMDA=61,120) =
1 5.40E15, 5.40E15, 5.40E15, 5.35E15, 5.35E15, 5.30E15, 5.25E15, START

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2 5.20E15, 5.15E15, 5.10E15, 5.05E15, 5.00E15, 4.95E15, 4.90E15, START
3 4.85E15, 4.80E15, 4.72E15, 4.64E15, 4.56E15, 4.48E15, 4.44E15, START
4 4.39E15, 4.34E15, 4.30E15, 4.25E15, 4.21E15, 4.17E15, 4.13E15, START
5 4.09E15, 4.05E15, 4.00E15, 3.95E15, 3.90E15, 3.85E15, 3.80E15, START
6 3.77E15, 3.74E15, 3.71E15, 3.68E15, 3.65E15, 3.62E15, 3.58E15, START
7 3.54E15, 3.50E15, 3.46E15, 3.42E15, 3.39E15, 3.36E15, 3.33E15, START
8 3.30E15, 3.26E15, 3.22E15, 3.18E15, 3.14E15, 3.10E15, 3.06E15, START
9 3.01E15, 2.97E15, 2.93E15, 2.88E15)
DATA ((KARASN2(LAMDA),LAMDA=1,60) =
1 5.0E-18, 1.1E-17, 1.2E-17, 1.4E-17, 1.5E-17, 1.6E-17, 1.8E-17, START
2 1.9E-17, 1.0E-18, 1.0E-18, 1.0E-18, 2.0E-21, 2.0E-21, 2.0E-21, START
3 2.0E-21, 45(0.0E-00))
DATA ((KARASN2(LAMDA),LAMDA=61,120) =
1 60(0.0E-00))
DATA ((KABSO3(LAMDA),LAMDA=1,60) =
1 1.5E-20, 3.0E-20, 5.0E-20, 9.0E-20, 1.7E-19, 3.2E-19, 6.0E-19, START
2 1.0E-18, 2.0E-18, 3.6E-18, 7.0E-18, 1.0E-17, 1.0E-17, 1.0E-17, START
3 3.6E-18, 1.6E-18, 8.3E-19, 6.0E-19, 4.5E-19, 3.2E-19, 5.0E-19, START
4 1.0E-18, 2.3E-18, 5.0E-18, 9.0E-18, 1.0E-17, 5.0E-18, 2.3E-18, START
5 1.3E-18, 7.0E-19, 2.0E-19, 8.0E-20, 2.0E-20, 1.0E-21, 1.0E-21, START
6 1.0E-21, 0.0E-00, 0.0E-00, 0.0E-00, 0.0E-00, 0.0E-00, 0.0E-00, START
7 0.0E-00, 0.0E-00, 1.0E-24, 1.3E-22, 2.0E-22, 3.3E-22, 5.0E-22, START
8 8.0E-22, 1.1E-21, 1.3E-21, 1.5E-21, 1.8E-21, 2.1E-21, 2.5E-21, START
9 2.9E-21, 3.4E-21, 4.0E-21, 4.7E-21)
DATA ((KABSO3(LAMDA),LAMDA=61,120) =
1 4.8E-21, 4.0E-21, 3.3E-21, 2.9E-21, 2.4E-21, 2.0E-21, 1.7E-21, START
2 1.5E-21, 1.2E-21, 1.1E-21, 7.8E-22, 5.0E-22, 3.2E-22, 2.0E-22, START
3 46(0.0E-00))
DATA ((KABSO2(LAMDA),LAMDA=1,120) =
1 6.0E-19, 6.0E-18, 1.4E-17, 2.0E-17, 2.3E-17, 2.3E-17, 2.1E-17, START
2 1.5E-17, 9.0E-18, 3.8E-18, 1.1E-18, 3.4E-19, 1.0E-20, 7.2E-18, START
3 1.3E-17, 8.8E-18, 3.3E-18, 5.3E-19, 1.8E-20, 2.8E-23, 1.6E-23, START
4 1.0E-23, 6.6E-24, 4.7E-24, 1.5E-24, 5.0E-25, 94(0.0))
DATA ((TABO2(JZTAB),JZTAB=1,87) =
1 1.61E09, 1.70E09, 1.79E09, 1.88E09, 1.98E09, 2.08E09, 2.20E09, START
2 2.32E09, 2.46E09, 2.60E09, 2.74E09, 2.89E09, 3.04E09, 3.22E09, START
3 3.41E09, 3.60E09, 3.81E09, 4.02E09, 4.26E09, 4.52E09, 4.78E09, START
4 5.15E09, 5.52E09, 6.00E09, 6.63E09, 7.26E09, 8.15E09, 9.04E09, START
5 1.01E10, 1.16E10, 1.31E10, 1.53E10, 1.75E10, 2.04E10, 2.50E10, START
6 2.96E10, 3.80E10, 4.64E10, 6.00E10, 8.01E10, 1.03E11, 1.38E11, START
7 1.74E11, 2.26E11, 3.12E11, 3.98E11, 5.61E11, 7.24E11, 1.08E12, START
8 1.54E12, 2.00E12, 3.06E12, 4.14E12, 6.04E12, 9.50E12, 1.30E13, START
9 1.90E13, 2.76E13, 3.98E13, 5.70E13, 8.06E13, 1.02E14, 1.54E14, START
1 2.10E14, 2.78E14, 3.68E14, 4.78E14, 6.16E14, 7.86E14, 9.98E14, START
2 1.27E15, 1.60E15, 2.02E15, 2.58E15, 3.30E15, 4.26E15, 5.52E15, START
3 7.22E15, 9.52E15, 1.27E16, 1.69E16, 2.28E16, 3.06E16, 3.80E16, START
4 5.64E16, 7.66E16, 7.66E16)
DATA ((TABO3(JZTAB),JZTAB=1,87) =
1 1.00E00, 1.30E00, 1.90E00, 2.40E00, 3.10E00, 4.00E00, 6.00E00, START
2 8.00E00, 1.05E01, 1.40E01, 1.95E01, 2.60E01, 3.50E01, 4.50E01, START
3 6.20E01, 9.00E01, 1.30E02, 1.80E02, 2.40E02, 3.40E02, 4.80E02, START
4 7.00E02, 1.10E03, 1.70E03, 2.20E03, 3.20E03, 5.00E03, 7.20E03, START
5 1.00E04, 1.50E04, 2.00E04, 3.00E04, 4.00E04, 5.80E04, 8.00E04, START
6 1.01E05, 1.60E05, 2.10E05, 3.00E05, 3.90E05, 5.00E05, 7.00E05, START

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7	9.20E05, 1.20E06, 1.70E06, 2.00E06, 2.60E06, 3.50E06, 4.50E06,	START
8	5.70E06, 7.50E06, 9.00E06, 1.10E07, 1.30E07, 1.70E07, 2.10E07,	START
9	2.60E07, 3.50E07, 4.80E07, 7.00E07, 1.00E08, 1.40E08, 1.90E08,	START
1	2.90E08, 4.00E08, 5.60E08, 8.50E08, 1.30E09, 2.00E09, 2.90E09,	START
2	4.10E09, 6.00E09, 1.00E10, 1.50E10, 2.20E10, 3.60E10, 5.60E10,	START
3	8.50E10, 1.40E11, 2.50E11, 6.00E11, 1.40E12, 3.00E12, 4.00E12,	START
4	5.00E12, 6.00E12, 6.00E12)	START
	IFLAG4 = 0	START
	IFLAG5 = 0	START
	DO 10 M1=3, NSPEC	START
10	READ (60,999) M2, (IATOM(ITCH,M2), ITCH=1,10)	START
	CONTINUE	START
	READ (60,994) T, TPRINT, TMAX1, TMAX2, TQUIT, IFLAG8,	START
1	IFLAG1, EQUIL, JOSHUA	START
	READ (60,993) LAT, LONG, TMONTH, TDAY, THOUR, TMIN, TSEC	START
	DO 20 M3=2, NSPEC	START
	READ (IUNIT,998) M4	START
	IF (M4 .EQ. 3) IFLAG6=1	START
	IF (M4 .EQ. 4) IFLAG7=1	START
	IF (M4 .EQ. 99) GO TO 30	START
	YNEW(M4) = 2.0	START
	READ (IUNIT,997) (YHOLD(M4,JZ2), JZ2=1, JZEND)	START
20	CONTINUE	START
	PRINT 996	START
	IFLAG9 = 1	START
	GO TO 9000	START
30	IF (IUNIT .EQ. 13) REWIND 13	START
	IF (IFLAG6 .EQ. 1 .AND. IFLAG7 .EQ. 1) GO TO 40	START
	IF (Z(1) .LE. 200.0 .AND. Z(JZEND) .GE. 30.0) GO TO 40	START
	PRINT 995	START
	IFLAG9 = 1	START
	GO TO 9000	START
40	DO 60 JZ3=1, JZEND	START
	DO 50 JZTAB=1, 87	START
	ZTAB = 202-2*JZTAB	START
	IF (ZTAB .GT. Z(JZ3)) GO TO 50	START
	Y3SUN(JZ3) = (TAB02(JZTAB-1)-TAB02(JZTAB))*(Z(JZ3)-ZTAB)/2.0	START
1	+ TAB02(JZTAB)	START
	Y4SUN(JZ3) = (TAB03(JZTAB-1)-TAB03(JZTAB))*(Z(JZ3)-ZTAB)/2.0	START
1	+ TAB03(JZTAB)	START
	GO TO 55	START
50	CONTINUE	START
	PRINT 995	START
	IFLAG9 = 1	START
	GO TO 9000	START
55	IF (IFLAG6 .EQ. 0) YHOLD(3, JZ3) = Y3SUN(JZ3)	START
	IF (IFLAG7 .EQ. 0) YHOLD(4, JZ3) = Y4SUN(JZ3)	START
60	CONTINUE	START
80	DO 85 M6=5, NSPEC	START
	IF (YNEW(M6) .GT. 1.0) GO TO 85	START
	DO 83 JZ6=1, JZEND	START
	YHOLD(M6, JZ6) = 5.0E-6*YHOLD(3, JZ6)	START
83	CONTINUE	START
85	CONTINUE	START

DO 110 ITC=1,10	START
CHECK = 0.0	START
DO 100 JZ=1,JZEND	START
SUMIN(ITC,JZ) = 0.0	START
DO 90 M=3,NSPEC	START
SUMIN(ITC,JZ) = SUMIN(ITC,JZ) + YHOLD(M,JZ)*IATOM(ITC,M)	START
90 CONTINUE	START
CHECK = CHECK + SUMIN(ITC,JZ)	START
100 CONTINUE	START
IF (CHECK .GT. 1.0) GO TO 110	START
ITCXX = ITC-1	START
GO TO 120	START
110 CONTINUE	START
120 TOLD = T	START
DO 150 M = 1,NSPEC	START
DO 140 JZ = 1,JZEND	START
YPRINT(M,JZ) = YHOLD(M,JZ)	START
YLAST(M,JZ) = YHOLD(M,JZ)	START
140 CONTINUE	START
150 CONTINUE	START
999 FORMAT(I2,2X,10(I1,1X))	START
998 FORMAT (I2)	START
997 FORMAT (7(E8.2,2X))	START
996 FORMAT (1H ,*NO END OF START PROFILES FOUND.*)	START
995 FORMAT (1H ,*THE ALTITUDES ARE OUTSIDE THE BOUNDS OF 30-200 KM. SO	START
1YOU'LL HAVE TO PUT IN YOUR OWN PROFILES FOR 02 AND 03.*)	START
994 FORMAT (5(E8.2,2X),2(I1,2X),E8.2,2X,I1)	START
993 FORMAT (2(E9.2,2X),5(I2,2X))	START
9000 RETURN	START
END	START -

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SUBROUTINE ZENANG
COMMON /A/      A(51)          ,ARK(4)          ,B(51)          ,ZENANG
1 BRK(4)        ,CRK(4)          ,F(20)          ,FF(20)         ,ZENANG
2 FLUX(120)     ,FLXINF(120)    ,FRATE(20)     ,FTERM(40)     ,ZENANG
3 FTERMW(40)    ,G(20)          ,GG(20)          ,HBR(20)       ,ZENANG
4 H2HOLD(20)    ,H3HOLD(20)     ,IATOM(10,20)    ,IGAIN(4)       ,ZENANG
5 IGA1NA(20,20) ,IGA1NB(20,20)  ,IGA1NC(20,20)  ,IGA1ND(20,20) ,ZENANG
6 ILOSS(4)      ,ILOSSA(20,20)  ,ILOSSB(20,20)  ,ILOSSC(20,20) ,ZENANG
7 ILOSSD(20,20) ,INFORM(30)     ,JPULL(20)      ,K(1000)       ,ZENANG
8 K0(51)        ,KABS(20,120)   ,KABS2(120)     ,KABS02(120)    ,ZENANG
9 KABS03(120)   ,KRK(80)        ,L1(51)         ,L2(51)         ,ZENANG
X L3(51)        ,LL1(21)        ,LL2(21)        ,LL3(21)        ,ZENANG
1 N(51)         ,NASRAS(1000)   ,NFTERM(20)     ,NTERM(20)     ,ZENANG
2 NUSRUS(400)   ,PHOLD(20,20)   ,PROHLD(71,20)  ,QOLD(20)       ,ZENANG
3 QRK(20)       ,R1(51)         ,R2(51)         ,R3(51)         ,ZENANG
4 RR1(21)       ,RR2(21)        ,RR3(21)        ,SUMIN(10,20)   ,ZENANG
5 TAB02(87)     ,TAB03(87)      ,TEMP(20)       ,TERM(100)      ,ZENANG
6 TERMW(100)    ,Y(20)          ,YHOLD(20,20)    ,YLAST(20,20)   ,ZENANG
7 YNEW(20)      ,YOLD(20)       ,YPRINT(20,20)  ,YSTART(20,20)  ,ZENANG
8 Y3SUN(20)     ,Y4SUN(20)     ,Z(20)          ,ZPRINT(20)     ,ZENANG
COMMON /B/      ALPHA , EQUIL , H , HCOUNT, IFLAG1, IFLAG2,
1 IFLAG3, IFLAG4, IFLAG5, IFLAG6, IFLAG7, IFLAG8, ZENANG
2 IFLAG9, IJZX , ITCXX, IUNIT , JCNTL, JFLAG2, ZENANG
3 JFLAG6, JOSHUA, JZEND , JZMAIN, LAT , LONG , ZENANG
4 NFREAC, NREAC , NSPEC , PI , T , TDAY , ZENANG
5 THOUR , TMAX1 , TMAX2 , TMIN , TMONTH, TOLD , ZENANG
6 TPRINT, TQUIT , TSEC , ZBOTUM, ZSTEP , ZTOP ZENANG
7 INTEGER HCOUNT,PHOLD,R1,R2,R3,RR1,RR2,RR3,RX1,RX2,RX3, ZENANG
1 TMONTH,TDAY,THOUR,TMIN,TSEC,TX ZENANG
REAL K0,N,KABS,K,KRK,LAT,LONG,K5,K5MAX,KABS02,KABS03,KABS2 ZENANG
IF (IFLAG3.NE. 0) GO TO 10 ZENANG
RAD = PI/180.0 ZENANG
DEC = 23.445*SINF((2.0*PI*(30.4*TMONTH+TDAY-80.0))/365.0) ZENANG
IFLAG3 = 1 ZENANG
PRINT 998 ZENANG
JCNTL = 0 ZENANG
THOLD = TPRINT ZENANG
TPRINT = 0 ZENANG
TZEN = 15.*ABSF(FLOATF(TSEC+60*(TMIN+60*THOUR))-43200.0)/3600.0 ZENANG
ALPHA = (1.0/RAD)*ACOSF(SINF(LAT*RAD)*SINF(DEC*RAD) ZENANG
+ COSF(LAT*RAD)*COSF(DEC*RAD)*COSF(TZEN*RAD)) ZENANG
1 CALL HANDLE ZENANG
JCNTL = 1 ZENANG
TPRINT = THOLD ZENANG
GO TO 100 ZENANG
10 IF (JOSHUA.EQ. 1) GO TO 100 ZENANG
TZEN = 15.*ABSF(FLOATF(TSEC+60*(TMIN+60*THOUR))-43200.0)/3600.0 ZENANG
ALPHA = (1.0/RAD)*ACOSF(SINF(LAT*RAD)*SINF(DEC*RAD) ZENANG
+ COSF(LAT*RAD)*COSF(DEC*RAD)*COSF(TZEN*RAD)) ZENANG
1 ZENANG
100 IF (ALPHA.GT. 90.0+SORTF(Z(1))) GO TO 9000 ZENANG
IF (ALPHA.GT. 90.0) GO TO 300 ZENANG
DO 200 JZ1=1,JZEND ZENANG
Y3SUN(JZ1) = YHOLD(3,JZ1) ZENANG
Y4SUN(JZ1) = YHOLD(4,JZ1) ZENANG

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200 CONTINUE	ZENANG
300 IF (Y3SUN(2) .GT. Y3SUN(1)) GO TO 310	ZENANG
PRINT 997	ZENANG
IFLAG9 = 1	ZENANG
GO TO 9000	ZENANG
310 IF (Y3SUN(1) .GT. 0.0) GO TO 320	ZENANG
H2HOLD(1) = 1.0	ZENANG
GO TO 330	ZENANG
320 H2HOLD(1) = (Z(2)-Z(1))/LOGF(Y3SUN(1)/Y3SUN(2))	ZENANG
330 IF (Y4SUN(2) .GT. Y4SUN(1)) GO TO 340	ZENANG
PRINT 996	ZENANG
IFLAG9 = 1	ZENANG
GO TO 9000	ZENANG
340 IF (Y4SUN(1) .GT. 0.0) GO TO 350	ZENANG
H3HOLD(1) = 1.0	ZENANG
GO TO 400	ZENANG
350 H3HOLD(1) = (Z(2)-Z(1))/LOGF(Y4SUN(1)/Y4SUN(2))	ZENANG
400 ADD3 = Y3SUN(1)*H2HOLD(1)	ZENANG
ADD4 = Y4SUN(1)*H3HOLD(1)	ZENANG
DO 410 JZ2=2,JZEND	ZENANG
ADD3 = ADD3 + (Y3SUN(JZ2-1)+Y3SUN(JZ2))*(Z(JZ2-1)-Z(JZ2))/2.0	ZENANG
ADD4 = ADD4 + (Y4SUN(JZ2-1)+Y4SUN(JZ2))*(Z(JZ2-1)-Z(JZ2))/2.0	ZENANG
H2HOLD(JZ2) = ADD3/Y3SUN(JZ2)	ZENANG
H3HOLD(JZ2) = ADD4/Y4SUN(JZ2)	ZENANG
410 CONTINUE	ZENANG
997 FORMAT(1H0,*THE TOP SCALE HEIGHT FOR O2 IS NEGATIVE*)	ZENANG
996 FORMAT(1H0,*THE TOP SCALE HEIGHT FOR O3 IS NEGATIVE*)	ZENANG
998 FORMAT(1H1,*-----STARTING VALUES-----*,/,	ZENANG
1 *(REACTION TERM BLOCK CONTAINS RATE COEFFICIENTS*)	ZENANG
9000 RETURN	ZENANG
END	ZENANG-

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SUBROUTINE PRODUC
COMMON /A/      A(51)      ,ARK(4)      ,B(51)      ,
1 BRK(4)      ,CRK(4)      ,F(20)      ,FF(20)      ,
2 FLUX(120)    ,FLXINF(120) ,FRATE(20)   ,FTERM(40)   ,
3 FTERMW(40)   ,G(20)      ,GG(20)      ,HBAR(20)   ,
4 H2HOLD(20)   ,H3HOLD(20) ,IATOM(10,20) ,IGAIN(4)    ,
5 IGAINGA(20,20) ,IGAINGB(20,20) ,IGAINGC(20,20) ,IGAINGD(20,20) ,
6 ILOSS(4)     ,ILOSSA(20,20) ,ILOSSB(20,20) ,ILOSSC(20,20) ,
7 ILOSSD(20,20) ,INFORM(30) ,JPULL(20)   ,K(1000)   ,
8 K0(51)       ,KABS(20,120) ,KABSN2(120) ,KABS02(120) ,
9 KABS03(120)  ,KRK(80)    ,L1(51)      ,L2(51)      ,
X L3(51)       ,LL1(21)    ,LL2(21)      ,LL3(21)      ,
1 N(51)        ,NASRAS(1000) ,NFTERM(20)   ,NTERM(20)   ,
2 NUSRU(400)   ,PHOLD(20,20) ,PROHLD(71,20) ,QOLD(20)    ,
3 QRK(20)      ,R1(51)     ,R2(51)      ,R3(51)      ,
4 RR1(21)      ,RR2(21)    ,RR3(21)      ,SUMIN(10,20) ,
5 TABO2(87)    ,TABO3(87)  ,TEMP(20)     ,TERM(100)   ,
6 TERMW(100)   ,Y(20)      ,YHOLD(20,20) ,YLAST(20,20) ,
7 YNEW(20)     ,YOLD(20)   ,YPRINT(20,20) ,YSTART(20,20) ,
8 Y3SUN(20)    ,Y4SUN(20)  ,Z(20)       ,ZPRINT(20)   ,
COMMON /B/     ALPHA , EQUIL , H      , HCOUNT , IFLAG1 , IFLAG2 ,
2 IFLAG3 , IFLAG4 , IFLAG5 , IFLAG6 , IFLAG7 , IFLAG8 ,
3 IFLAG9 , IJZX , ITCX , IUNIT , JCNTRL , JFLAG2 ,
4 JFLAG6 , JOSHUA , JZEND , JZMAIN , LAT , LONG ,
5 NFREAC , NREAC , NSPEC , PI , T , TDAY ,
6 THOUR , TMAX1 , TMAX2 , TMIN , TMONTH , TOLD ,
7 TPRINT , TQUIT , TSEC , ZBOTUM , ZSTEP , ZTOP ,
INTEGER HCOUNT,PHOLD,R1,R2,R3,RR1,RR2,RR3,RX1,RX2,RX3,
1 TMONTH,TDAY,THOUR,TMIN,TSEC,TX
REAL K0,N,KABS,K,KRK,LAT,LONG,K5,K5MAX,KABS02,KABS03,KABSN2
CALL Q9EXUN
IF (NFREAC.EQ. 0) GO TO 9000
ALPHAR = ALPHA*PI/180.0
REARTH = 6371.0
IF (ALPHA.GT. 90.0) GO TO 100
C THIS CALCULATION DONE USING EQN. 53 IN SWIDER, PLANET. SPACE SCI.,
C VOL. 12, NO. 8, 1964.
PI2 = (PI/2.0)**2
XX = (REARTH+Z(JZMAIN))/H2HOLD(JZMAIN)
AXLE = (1.0-PI2*(0.115+1.0/LOGF(PI*XX/2.0)))/PI2**2
FO2 = EXPF((ALPHAR**2/2.0)/(1.0-ALPHAR**2*(0.115+AXLE*ALPHAR**2)))
XX = (REARTH+Z(JZMAIN))/H3HOLD(JZMAIN)
AXLE = (1.0-PI2*(0.115+1.0/LOGF(PI*XX/2.0)))/PI2**2
FO3 = EXPF((ALPHAR**2/2.0)/(1.0-ALPHAR**2*(0.115+AXLE*ALPHAR**2)))
GO TO 300
100 IF (ALPHA.GT. 90.0+SORTF(Z(JZMAIN))) GO TO 1000
V = (6370.0+Z(JZMAIN))*SINF(ALPHAR)-6370.0
IF (V.GE. Z(1)) GO TO 130
IF (V.LE. Z(JZEND)) GO TO 140
DO 110 JZ1=1,JZEND
IF (V.GT. Z(JZ1)) GO TO 120
110 CONTINUE
GO TO 140
120 H02 = (H2HOLD(JZ1)-H2HOLD(JZ1-1))*(V-Z(JZ1-1))/(Z(JZ1)-Z(JZ1-1))

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1      +H2HOLD(JZ1-1)
HO3 = (H3HOLD(JZ1)-H2HOLD(JZ1-1))*(V-Z(JZ1-1))/(Z(JZ1)-Z(JZ1-1))
1      +H3HOLD(JZ1-1)
GO TO 150
130 HO2 = H2HOLD(JZ1)
HO3 = H3HOLD(JZ1)
GO TO 150
140 HO2 = H2HOLD(JZEND)
HO3 = H3HOLD(JZEND)
150 XO2 = (ALPHA-90.0)/SQRTF(HO2)
XO3 = (ALPHA-90.0)/SQRTF(HO3)
IF (XO2 .GT. 2.5) GO TO 180
ERFO2 = XO2
FXX = 1.0
DO 160 IERF=1,50
FXX = FXX*IERF
TXX = (-1)**IERF*XO2**(2*IERF+1)/(FXX*(2*IERF+1))
ERFO2 = ERFO2 + TXX
IF (ABS(TXX) .LT. ABS(ERFO2*1.0E-4)) GO TO 170
160 CONTINUE
ERFO2 = ERFO2*2.0/SQRTF(P1)
GO TO 190
180 ERFO2 = 1.00
190 IF (XO3 .GT. 2.5) GO TO 220
ERFO3 = XO3
FXX = 1.0
DO 200 IERF2=1,50
FXX = FXX*IERF2
TXX = (-1)**IERF2*XO3**(2*IERF2+1)/(FXX*(2*IERF2+1))
ERFO3 = ERFO3 + TXX
IF (ABS(TXX) .LT. ABS(ERFO3*1.0E-4)) GO TO 210
200 CONTINUE
ERFO3 = ERFO3*2.0/SQRTF(P1)
GO TO 230
220 ERFO3 = 1.0
230 FO2 = (101.4/SQRTF(HO2))*(1.0+ERFO2)
FO3 = (101.4/SQRTF(HO3))*(1.0+ERFO3)
300 DO 310 LAMDA1=1,120
FLUX(LAMDA1) = FLXINF(LAMDA1)*EXP(
1 -KABSO2(LAMDA1)*Y3SUN(JZMAIN)*H2HOLD(JZMAIN)*1.0E5*FO2
1 -KABSO3(LAMDA1)*Y4SUN(JZMAIN)*H3HOLD(JZMAIN)*1.0E5*FO3)
310 CONTINUE
DO 330 II=1,NFREAC
FRATE(II) = 0.0
DO 320 LAMDA2=1,120
FRATE(II) = FRATE(II) + KABS(II,LAMDA2)*FLUX(LAMDA2)
320 CONTINUE
330 CONTINUE
GO TO 9000
1000 DO 1010 II = 1,NFREAC
FRATE(II) = 0.0
1010 CONTINUE
9000 CALL R9EXUN
RETURN
END

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PRODUC-

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SUBROUTINE PHYSICS
COMMON /A/      A(51)      ,ARK(4)      ,B(51)      , PHYSICS
1 BRK(4)      ,CRK(4)      ,F(20)      ,FF(20)      , PHYSICS
2 FLUX(120)   ,FLXINF(120) ,FRATE(20) ,FTERM(40) , PHYSICS
3 FTERMW(40)  ,G(20)      ,GG(20)      ,HBAR(20) , PHYSICS
4 H2HOLD(20)  ,H3HOLD(20) ,IATOM(10,20) ,IGAIN(4) , PHYSICS
5 IGAINA(20,20) ,IGAINB(20,20) ,IGAINC(20,20) ,IGAIND(20,20) , PHYSICS
6 ILOSS(4)    ,ILOSSA(20,20) ,ILOSSB(20,20) ,ILOSSC(20,20) , PHYSICS
7 ILOSSD(20,20) ,INFORM(30) ,JPULL(20) ,K(1000) , PHYSICS
8 K0(51)      ,KABS(20,120) ,KABSN2(120) ,KABSO2(120) , PHYSICS
9 KABSO3(120)  ,KPK(80)    ,L1(51)      ,L2(51)      , PHYSICS
X L3(51)      ,LL1(21)     ,LL2(21)     ,LL3(21)     , PHYSICS
1 N(51)       ,NASRAS(1000) ,NFTERM(20) ,NTERM(20) , PHYSICS
2 NUSRUS(400) ,PHOLD(20,20) ,PROHLD(71,20) ,QOLD(20) , PHYSICS
3 QRK(20)     ,R1(51)      ,R2(51)      ,R3(51)      , PHYSICS
4 RR1(21)     ,RR2(21)     ,RR3(21)     ,SUMIN(10,20) , PHYSICS
5 TABO2(87)   ,TABO3(87)   ,TEMP(20)    ,TERM(100) , PHYSICS
6 TERMW(100)  ,Y(20)      ,YHOLD(20,20) ,YLAST(20,20) , PHYSICS
7 YNEW(20)    ,YOLD(20)    ,YPRINT(20,20) ,YSTART(20,20) , PHYSICS
8 Y3SUN(20)   ,Y4SUN(20)   ,Z(20)      ,ZPRINT(20) , PHYSICS
COMMON /B/    ALPHA , EQUIL , H , HCOUNT , IFLAG1 , IFLAG2 , PHYSICS
2 IFLAG3 , IFLAG4 , IFLAG5 , IFLAG6 , IFLAG7 , IFLAG8 , PHYSICS
3 IFLAG9 , IJZX , ITCHXX , IUNIT , JCNTRL , JFLAG2 , PHYSICS
4 JFLAG6 , JOSHUA , JZEND , JZMAIN , LAT , LONG , PHYSICS
5 NFREAC , NREAC , NSPEC , PI , T , TDAY , PHYSICS
6 THOUR , TMAX1 , TMAX2 , TMIN , TMONTH , TOLD , PHYSICS
7 TPRINT , TQUIT , TSEC , ZBOTUM , ZSTEP , ZTOP , PHYSICS
INTEGER HCOUNT,PHOLD,R1,R2,R3,RR1,RR2,RR3,RX1,RX2,RX3, PHYSICS
1 TMONTH,TDAY,THOUR,TMIN,TSEC,TX PHYSICS
REAL K0,N,KABS,K,KRK,LAT,LONG,K5,K5MAX,KABSO2,KABSO3,KABSN2 PHYSICS
DO 800 M1=3,NSPEC PHYSICS
IIX = (M1-3)*NFREAC PHYSICS
IIFX = (M1-3)*NFREAC PHYSICS
NNSTOP = NTERM(M1) + NFTERM(M1) PHYSICS
NTX = NTERM(M1) PHYSICS
DO 700 JZ1=1,JZEND PHYSICS
DO 100 ILOOK1=1,4 PHYSICS
ILOSS(ILOOK1) = IGAIN(ILOOK1) = 0 PHYSICS
100 CONTINUE PHYSICS
DO 600 ILOOK2=1,4 PHYSICS
ILMAX = IGMAX = 0 PHYSICS
TLMAX = TGMAX = 0.0 PHYSICS
DO 500 NN=1,NNSTOP PHYSICS
IF (NN .GT. NTX) GO TO 110 PHYSICS
NX = NASRAS(IIX+NN) PHYSICS
GO TO 150 PHYSICS
110 NX = NUSRUS(IIFX+NN-NTX) PHYSICS
150 ILX = ILOOK2-1 PHYSICS
IF (NN .GT. NTX .AND. NX .GT. NFREAC) GO TO 300 PHYSICS
IF (NN .LE. NTX .AND. NX .GT. NREAC) GO TO 300 PHYSICS
DO 200 ILOOK3=1,ILX PHYSICS
IF (NN .GT. NTX) GO TO 180 PHYSICS
IF (NX .EQ. ILOSS(ILOOK3)) GO TO 500 PHYSICS
GO TO 200 PHYSICS

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180 IF (NX+NREAC .EQ. ILOSS(ILOOK3)) GO TO 500      PHYSICS
200 CONTINUE                                         PHYSICS
250 IF (NN .GT. NTX) GO TO 260                      PHYSICS
    IF (PROHLD(NX,JZ1) .GT. TLMAX) GO TO 270        PHYSICS
    GO TO 500                                         PHYSICS
260 IF (PROHLD(NX+NREAC,JZ1) .LE. TLMAX) GO TO 500  PHYSICS
    TLMAX = PROHLD(NX+NREAC,JZ1)                   PHYSICS
    ILMAX = NX+NREAC                                PHYSICS
    GO TO 500                                         PHYSICS
270 TLMAX = PROHLD(NX,JZ1)                           PHYSICS
    ILMAX = NX                                       PHYSICS
    GO TO 500                                         PHYSICS
300 IF (NN .GT. NTX) GO TO 310                      PHYSICS
    NX = NX-NREAC                                    PHYSICS
    GO TO 320                                         PHYSICS
310 NX = NX-NFREAC                                    PHYSICS
320 DO 400 ILOOK4=1,ILX                             PHYSICS
    IF (NN .GT. NTX) GO TO 350                      PHYSICS
    IF (NX .EQ. IGAIN(ILOOK4)) GO TO 500            PHYSICS
    GO TO 400                                         PHYSICS
350 IF (NX+NREAC .EQ. IGAIN(ILOOK4)) GO TO 500      PHYSICS
400 CONTINUE                                         PHYSICS
    IF (NN .GT. NTX) GO TO 410                      PHYSICS
    IF (PROHLD(NX,JZ1) .GT. TGMAX) GO TO 420        PHYSICS
    GO TO 500                                         PHYSICS
410 IF (PROHLD(NX+NREAC,JZ1) .LE. TGMAX) GO TO 500  PHYSICS
    TGMAX = PROHLD(NX+NREAC,JZ1)                   PHYSICS
    IGMAX = NX+NREAC                                PHYSICS
    GO TO 500                                         PHYSICS
420 TGMAX = PROHLD(NX,JZ1)                           PHYSICS
    IGMAX = NX                                       PHYSICS
500 CONTINUE                                         PHYSICS
    IF (ILOOK2 .EQ. 1) GO TO 550                   PHYSICS
    IF (TLMAX .GE. 0.1*BIGL) ILOSS(ILOOK2) = ILMAX  PHYSICS
    IF (TGMAX .GE. 0.1*BIGG) IGAIN(ILOOK2) = IGMAX  PHYSICS
    GO TO 600                                         PHYSICS
550 ILOSS(1) = ILMAX                                PHYSICS
    IGAIN(1) = IGMAX                                PHYSICS
    BIGL = TLMAX                                     PHYSICS
    BIGG = TGMAX                                     PHYSICS
600 CONTINUE                                         PHYSICS
    IF (ILOSS(1) .EQ. 0) GO TO 610                  PHYSICS
    ILOSSA(M1,JZ1) = ILOSS(1)+100                   PHYSICS
    ILOSSB(M1,JZ1) = ILOSS(2)+100                   PHYSICS
    ILOSSC(M1,JZ1) = ILOSS(3)+100                   PHYSICS
    ILOSSD(M1,JZ1) = ILOSS(4)+100                   PHYSICS
    GO TO 620                                         PHYSICS
610 ILOSSA(M1,JZ1)=ILOSSB(M1,JZ1)=ILOSSC(M1,JZ1)=ILOSSD(M1,JZ1) = -1 PHYSICS
620 IF (IGAIN(1) .EQ. 0) GO TO 630                  PHYSICS
    IGAINA(M1,JZ1) = IGAIN(1)+100                   PHYSICS
    IGAINB(M1,JZ1) = IGAIN(2)+100                   PHYSICS
    IGAINC(M1,JZ1) = IGAIN(3)+100                   PHYSICS
    IGAIND(M1,JZ1) = IGAIN(4)+100                   PHYSICS
    GO TO 700                                         PHYSICS
630 IGAINA(M1,JZ1)=IGAINB(M1,JZ1)=IGAINC(M1,JZ1)=IGAIND(M1,JZ1) = -1 PHYSICS
700 CONTINUE                                         PHYSICS
800 CONTINUE                                         PHYSICS
    RETURN                                           PHYSICS
END

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SUBROUTINE HANDLE
COMMON /A/      A(51)      ,ARK(4)      ,B(51)      , HANDLE
1 BRK(4)      ,CRK(4)      ,F(20)      ,FF(20)      , HANDLE
2 FLUX(120)    ,FLXINF(120) ,FRATE(20)   ,FTERM(40)   , HANDLE
3 FTERMW(40)   ,G(20)      ,GG(20)      ,HBAR(20)   , HANDLE
4 HZHOLD(20)   ,H3HOLD(20) ,IATOM(10,20) ,IGAIN(4)   , HANDLE
5 IGAING(20,20) ,IGAINB(20,20) ,IGAINC(20,20) ,IGAIND(20,20) , HANDLE
6 ILOSS(4)     ,ILOSSA(20,20) ,ILOSSB(20,20) ,ILOSSC(20,20) , HANDLE
7 ILOSSD(20,20) ,INFORM(30) ,JPULL(20)    ,K(1000)   , HANDLE
8 KO(51)      ,KABS(20,120) ,KABSN2(120)  ,KABSO2(120) , HANDLE
9 KABSO3(120)  ,KRK(80)    ,L1(51)      ,L2(51)      , HANDLE
X L3(51)      ,LL1(21)    ,LL2(21)    ,LL3(21)    , HANDLE
1 N(51)      ,NASRAS(1000) ,NFTERM(20)   ,NTERM(20)   , HANDLE
2 NUSRUS(400) ,PHOLD(20,20) ,PROHLD(71,20) ,QOLD(20)   , HANDLE
3 QRK(20)     ,R1(51)     ,R2(51)     ,R3(51)     , HANDLE
4 RR1(21)    ,RR2(21)    ,RR3(21)    ,SUMIN(10,20) , HANDLE
5 TABO2(87)  ,TABO3(87)  ,TEMP(20)   ,TERM(100)   , HANDLE
6 TERMW(100) ,Y(20)      ,YHOLD(20,20) ,YLAST(20,20) , HANDLE
7 YNEW(20)   ,YOLD(20)   ,YPRINT(20,20) ,YSTART(20,20) , HANDLE
8 Y3SUN(20)  ,Y4SUN(20)  ,Z(20)      ,ZPRINT(20)   , HANDLE
COMMON /B/    ALPHA , EQUIL , H      , HCOUNT , IFLAG1 , IFLAG2 ,
2             IFLAG3 , IFLAG4 , IFLAG5 , IFLAG6 , IFLAG7 , IFLAG8 ,
3             IFLAG9 , IJZX , ICHXX , IUNIT , JCNTRL , JFLAG2 ,
4             JFLAG6 , JOSHUA , JZEND , JZMAIN , LAT , LONG ,
5             NFREAC , NREAC , NSPEC , P1 , T , TDAY ,
6             THOUR , TMAX1 , TMAX2 , TMIN , TMONTH , TOLD ,
7             TPRINT , TQUIT , TSEC , ZBOTUM , ZSTEP , ZTOP
INTEGER HCOUNT,PHOLD,R1,R2,R3,RR1,RR2,RR3,RX1,RX2,RX3,
1 TMONTH,TDAY,THOUR,TMIN,TSEC,TX
REAL KO,N,KABS,K,KRK,LAT, LONG,K5,K5MAX,KABSO2,KABSO3,KABSN2
TX=TPRINT+TSEC+TMIN*60+THOUR*3600+TDAY*86400+TMONTH*2592000
TMONTH = TX/2592000
TX = TX-TMONTH*2592000
TDAY = TX/86400
TX = TX - TDAY*86400
THOUR = TX/3600
TX = TX - THOUR*3600
TMIN = TX/60
TX = TX - TMIN*60
TSEC = TX
ITSEC = TSEC + 100
ITMIN = TMIN + 100
ITHOUR = THOUR + 100
ITDAY = TDAY + 100
PRINT 999, JCNTRL,ITHOUR,ITMIN,ITSEC,ITDAY,TMONTH
ITIME=KLOCK(1)
TIME=ITIME/1000.
PRINT 966,TIME
PRINT 998, T
PRINT 997, ALPHA
PRINT 994
NTREAC = NREAC + NFREAC
IF (NTREAC .LT. 8) GO TO 10
PRINT 993

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IF (NTREAC .LT. 16) GO TO 10	HANDLE
PRINT 992	HANDLE
IF (NTREAC .LT. 24) GO TO 10	HANDLE
PRINT 991	HANDLE
IF (NTREAC .LT. 32) GO TO 10	HANDLE
PRINT 965	HANDLE
IF (NTREAC .LT. 40) GO TO 10	HANDLE
PRINT 964	HANDLE
IF (NTREAC .LT. 48) GO TO 10	HANDLE
PRINT 963	HANDLE
IF (NTREAC .LT. 56) GO TO 10	HANDLE
PRINT 962	HANDLE
IF (NTREAC .LT. 64) GO TO 10	HANDLE
PRINT 961	HANDLE
10 DO 20 JZ = 1,JZEND	HANDLE
PRINT 982, Z(JZ), HBAR(JZ), (PROHLD(I1,JZ),I1=1,7)	HANDLE
IF (NTREAC .LT. 8) GO TO 20	HANDLE
PRINT 989, (PROHLD(I2,JZ),I2=8,15)	HANDLE
IF (NTREAC .LT. 16) GO TO 20	HANDLE
PRINT 988, (PROHLD(I3,JZ),I3=16,23)	HANDLE
IF (NTREAC .LT. 24) GO TO 20	HANDLE
PRINT 987, (PROHLD(I4,JZ),I4=24,31)	HANDLE
IF (NTREAC .LT. 32) GO TO 20	HANDLE
PRINT 989, (PROHLD(I2,JZ),I2=32,39)	HANDLE
IF (NTREAC .LT. 40) GO TO 20	HANDLE
PRINT 988, (PROHLD(I3,JZ),I3=40,47)	HANDLE
IF (NTREAC .LT. 48) GO TO 20	HANDLE
PRINT 987, (PROHLD(I4,JZ),I4=48,55)	HANDLE
IF (NTREAC .LT. 56) GO TO 20	HANDLE
PRINT 989, (PROHLD(I2,JZ),I2=56,63)	HANDLE
IF (NTREAC .LT. 64) GO TO 20	HANDLE
PRINT 988, (PROHLD(I3,JZ),I3=64,72)	HANDLE
20 CONTINUE	HANDLE
PRINT 986	HANDLE
IF (NSPEC .LT. 10) GO TO 30	HANDLE
PRINT 985	HANDLE
IF (NSPEC .LT. 18) GO TO 30	HANDLE
PRINT 984	HANDLE
IF (NSPEC .LT. 26) GO TO 30	HANDLE
PRINT 983	HANDLE
30 DO 40 JJZ=1,JZEND	HANDLE
PRINT 990, ZPRINT(JJZ), (YPRINT(I5,JJZ),I5=2,9)	HANDLE
IF (NSPEC .LT. 10) GO TO 40	HANDLE
PRINT 989, (YPRINT(I6,JJZ),I6=10,17)	HANDLE
IF (NSPEC .LT. 18) GO TO 40	HANDLE
PRINT 988, (YPRINT(I7,JJZ),I7=18,25)	HANDLE
IF (NSPEC .LT. 26) GO TO 40	HANDLE
PRINT 987, (YPRINT(I8,JJZ),I8=26,33)	HANDLE
40 CONTINUE	HANDLE
IF (JCNTRL .EQ. 0) GO TO 9000	HANDLE
PRINT 975	HANDLE
IF (NSPEC .LT. 10) GO TO 50	HANDLE
PRINT 974	HANDLE
IF (NSPEC .LT. 18) GO TO 50	HANDLE

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      PRINT 973
      IF (NSPEC .LT. 26) GO TO 50
      PRINT 972
50 DO 60 JZ3=1,JZEND
      PRINT 971,ZPRINT(JZ3),(ILOSSA(M1,JZ3),ILOSSB(M1,JZ3),
1 ILOSSC(M1,JZ3),ILOSSD(M1,JZ3),M1=2,9)
      IF (NSPEC .LT. 10) GO TO 60
      PRINT 970, (ILOSSA(M2,JZ3),ILOSSB(M2,JZ3),ILOSSC(M2,JZ3),
1 ILOSSD(M2,JZ3),M2=10,17)
      IF (NSPEC .LT. 18) GO TO 60
      PRINT 969, (ILOSSA(M3,JZ3),ILOSSB(M3,JZ3),ILOSSC(M3,JZ3),
1 ILOSSD(M3,JZ3),M3=18,25)
      IF (NSPEC .LT. 26) GO TO 60
      PRINT 968, (ILOSSA(M4,JZ3),ILOSSB(M4,JZ3),ILOSSC(M4,JZ3),
1 ILOSSD(M4,JZ3),M4=26,33)
60 CONTINUE
      PRINT 967
      IF (NSPEC .LT. 10) GO TO 70
      PRINT 974
      IF (NSPEC .LT. 18) GO TO 70
      PRINT 973
      IF (NSPEC .LT. 26) GO TO 70
      PRINT 972
70 DO 80 JZ4=1,JZEND
      PRINT 971,ZPRINT(JZ4),(IGAINA(M5,JZ4),IGAINB(M5,JZ4),
1 IGAINC(M5,JZ4),IGAIND(M5,JZ4),M5=2,9)
      IF (NSPEC .LT. 10) GO TO 80
      PRINT 970,(IGAINA(M6,JZ4),IGAINB(M6,JZ4),IGAINC(M6,JZ4),
1 IGAIND(M6,JZ4),M6=10,17)
      IF (NSPEC .LT. 18) GO TO 80
      PRINT 969,(IGAINA(M7,JZ4),IGAINB(M7,JZ4),IGAINC(M7,JZ4),
1 IGAIND(M7,JZ4),M7=18,25)
      IF (NSPEC .LT. 26) GO TO 80
      PRINT 968,(IGAINA(M8,JZ4),IGAINB(M8,JZ4),IGAINC(M8,JZ4),
1 IGAIND(M8,JZ4),M8=26,33)
80 CONTINUE
      IF (JZEND .GT. 7) GO TO 90
      WRITE (13,899) (M,(YHOLD(M,JZ),JZ=1,7),M=3,NSPEC),99
      GO TO 110
90 IF (JZEND .GT. 14) GO TO 100
      WRITE (13,898) (M,(YHOLD(M,JZ),JZ=1,14),M=3,NSPEC),99
      GO TO 110
100 WRITE (13,897) (M,(YHOLD(M,JZ),JZ=1,20),M=3,NSPEC),99
110 CONTINUE
      REWIND 13
897 FORMAT(I2,/,2(7(E8.2,2X),/),6(E8.2,2X))
898 FORMAT(I2,/,7(E8.2,2X),/,7(E8.2,2X))
899 FORMAT(I2,/,7(E8.2,2X))
961 FORMAT(1H , *
1M(66) TERM(67) TERM(68) TERM(64) TERM(65) TERHANDLE
2(71)*) TERM(69) TERM(70) TERMHANDLE
962 FORMAT(1H , *
1(58) TERM(59) TERM(60) TERM(56) TERM(57) TERMHANDLE
263)*) TERM(61) TERM(62) TERM(63) TERMHANDLE

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963 FORMAT(1H , *
1RM(50) TERM(51) TERM(52) TERM(48) TERM(49) TEHANDLE
2M(55)* TERM(53) TERM(54) TERHANDLE
HANDLE
964 FORMAT(1H , *
1M(42) TERM(43) TERM(44) TERM(40) TERM(41) TERHANDLE
2(47)* TERM(45) TERM(46) TERHANDLE
HANDLE
965 FORMAT(1H , *
1(34) TERM(35) TERM(36) TERM(32) TERM(33) TERHANDLE
2(47)* TERM(37) TERM(38) TERHANDLE
HANDLE
966 FORMAT(1X,*COMPUTER TIME= *,F9.3,* SECONDS*)
HANDLE
967 FORMAT(1H1,*MAJOR PRODUCTION REACTIONS-----*,/* HEIGHT NO. HANDLE
1 2 NO. 3 NO. 4 NO. 5 NO. 6
2 NO. 7 NO. 8 NO. 9*)
HANDLE
968 FORMAT(1H ,8X,8(3X,I2,*/,*,2(I2,*,*),I2))
HANDLE
969 FORMAT(1H ,7X,8(3X,I2,*/,*,2(I2,*,*),I2))
HANDLE
970 FORMAT(1H ,6X,8(3X,I2,*/,*,2(I2,*,*),I2))
HANDLE
971 FORMAT(1H0,F6.1,2X,8(I2,*/,*,2(I2,*,*),I2,3X))
HANDLE
972 FORMAT(1H ,* NO. 26 NO. 27 NO. 28
1 NO. 29 NO. 30 NO. 31 NO. 32 NO. 33*)
HANDLE
973 FORMAT(1H ,* NO. 18 NO. 19 NO. 20
1 NO. 21 NO. 22 NO. 23 NO. 24 NO. 25*)
HANDLE
974 FORMAT(1H ,* NO. 10 NO. 11 NO. 12
1NO. 13 NO. 14 NO. 15 NO. 16 NO. 17*)
HANDLE
975 FORMAT(1H1,*MAJOR DESTRUCTION REACTIONS-----*,/* HEIGHT NO. HANDLE
1 2 NO. 3 NO. 4 NO. 5 NO. 6
2 NO. 7 NO. 8 NO. 9*)
HANDLE
982 FORMAT(1H0,F6.1,2X,E10.4,3X,7(E10.3,3X))
HANDLE
983 FORMAT(1H ,* Y(26) Y(27) Y(28)
1(29) Y(30) Y(31) Y(32) Y(33)*
HANDLE
984 FORMAT(1H ,* Y(18) Y(19) Y(20) Y(21)
121) Y(22) Y(23) Y(24) Y(25)*
HANDLE
985 FORMAT(1H ,* Y(10) Y(11) Y(12) Y(13)
13) Y(14) Y(15) Y(16) Y(17)*
HANDLE
986 FORMAT(1H1,/* SPECIES DENSITIES-----*,/* HEIGHT Y(2)
1(3) Y(4) Y(5) Y(6) Y(7)
18) Y(9)*
HANDLE
987 FORMAT(1H ,12X,8(E10.3,3X))
HANDLE
988 FORMAT(1H ,11X,5(E10.3,3X))
HANDLE
989 FORMAT(1H ,10X,5(E10.3,3X))
HANDLE
990 FORMAT(1H0,F6.1,2X,F11.8,3X,7(E10.3,3X))
HANDLE
991 FORMAT(1H ,* TERM(24) TERM(25) TEHANDLE
1RM(26) TERM(27) TERM(28) TERM(29) TERM(30) TERHANDLE
2M(31)*
HANDLE
992 FORMAT(1H ,* TERM(16) TERM(17) TERHANDLE
1M(18) TERM(19) TERM(20) TERM(21) TERM(22) TERHANDLE
2(23)*
HANDLE
993 FORMAT(1H ,* TERM(8) TERM(9) TERM(10) TERHANDLE
1(11) TERM(12) TERM(13) TERM(14) TERM(15)*
HANDLE
994 FORMAT(1H0,*REACTION TERMS-----*,/* HEIGHT STEP SIZE TERHANDLE
1(1) TERM(2) TERM(3) TERM(4) TERM(5) TERM(HANDLE
26) TERM(7)*
HANDLE
997 FORMAT(1H ,*ZENITH ANGLE = *,F6.2,* DEGREES*)
HANDLE
998 FORMAT(1H ,*RUNNING TIME = *,E10.3,* SECONDS*)
HANDLE
999 FORMAT(11,*LOCAL TIME (HOURS,MINUTES,SECONDS) = *,I2,*/,*,I2,*/,*,I2HANDLE
1,* ON DAY NUMBER *,I2,*, MONTH NUMBER *,I3)
HANDLE
9000 RETURN
HANDLE
END
HANDLE-

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SUBROUTINE RUNKUT
COMMON /A/ A(51) ,*RK(4) ,B(51) , RUNKUT
1 BRK(4) ,CRK(4) ,F(20) ,FF(20) , RUNKUT
2 FLUX(120) ,FLXINF(120) ,FRATE(20) ,FTERM(40) , RUNKUT
3 FTERMW(40) ,G(20) ,GG(20) ,HBAR(20) , RUNKUT
4 H2HOLD(20) ,H3HOLD(20) ,IATOM(10,20) ,IGAIN(4) , RUNKUT
5 IGAINA(20,20) ,IGAINB(20,20) ,IGAINC(20,20) ,IGAIND(20,20) , RUNKUT
6 ILOSS(4) ,ILOSSA(20,20) ,ILOSSB(20,20) ,ILOSSC(20,20) , RUNKUT
7 ILOSSD(20,20) ,INFORM(30) ,JPULL(20) ,K(1000) , RUNKUT
8 K0(51) ,KABS(20,120) ,KABS2(120) ,KABS02(120) , RUNKUT
9 KABS03(120) ,KRK(80) ,L1(51) ,L2(51) , RUNKUT
X L3(51) ,LL1(21) ,LL2(21) ,LL3(21) , RUNKUT
1 N(51) ,NASRAS(1000) ,NFTERM(20) ,NTERM(20) , RUNKUT
2 NUSRUS(400) ,PHOLD(20,20) ,PROHLD(71,20) ,QOLD(20) , RUNKUT
3 GRK(20) ,R1(51) ,R2(51) ,R3(51) , RUNKUT
4 RR1(21) ,RR2(21) ,RR3(21) ,SUMIN(10,20) , RUNKUT
5 TAB02(87) ,TAB03(87) ,TEMP(20) ,TERM(100) , RUNKUT
6 TERMW(100) ,Y(20) ,YHOLD(20,20) ,YLAST(20,20) , RUNKUT
7 YNEW(20) ,YOLD(20) ,YPRINT(20,20) ,YSTART(20,20) , RUNKUT
8 Y3SUN(20) ,Y4SUN(20) ,Z(20) ,ZPRINT(20) , RUNKUT
COMMON /B/ ALPHA , EQUIL , H , HCOUNT , IFLAG1 , IFLAG2 ,
2 IFLAG3 , IFLAG4 , IFLAG5 , IFLAG6 , IFLAG7 , IFLAG8 , RUNKUT
3 IFLAG9 , IJZX , ITCHXX , IUNIT , JCNTL , JFLAG2 , RUNKUT
4 JFLAG6 , JOSHUA , JZEND , JZMAIN , LAT , LONG , RUNKUT
5 NFREAC , NREAC , NSPEC , PI , T , TODAY , RUNKUT
6 THOUR , TMAX1 , TMAX2 , TMIN , TMONTH , TOLD , RUNKUT
7 TPRINT , TQUIT , TSEC , ZBOTUM , ZSTEP , ZTOP , RUNKUT
INTEGER HCOUNT , PHOLD , R1 , R2 , R3 , RR1 , RR2 , RR3 , RX1 , RX2 , RX3 ,
1 TMONTH , TODAY , THOUR , TMIN , TSEC , TX , RUNKUT
REAL K0 , N , KABS , K , KRK , LAT , LONG , K5 , K5MAX , KABS02 , KABS03 , KABS2 , RUNKUT
CALL Q9EXUN , RUNKUT
H = HBAR(JZMAIN)*3.0 , RUNKUT
10 TCHECK = T-TOLD+H , RUNKUT
IF (TCHECK .LT. TPRINT-1.0E-6) GO TO 20 , RUNKUT
IF (TCHECK .GT. TPRINT+1.0E-6) H = TPRINT-T+TOLD , RUNKUT
IFLAG2 = 1 , RUNKUT
20 DO 30 M1=2,NSPEC , RUNKUT
YOLD(M1) = Y(M1) , RUNKUT
QOLD(M1) = GRK(M1) , RUNKUT
30 CONTINUE , RUNKUT
40 DO 90 JRK=1,4 , RUNKUT
DO 50 I1=1,NREAC , RUNKUT
TERM(I1+NREAC) = K(I1*JZEND-IJZX)*Y(L1(I1))*Y(L2(I1))*Y(L3(I1)) , RUNKUT
TERM(I1) = TERM(I1+NREAC) , RUNKUT
50 CONTINUE , RUNKUT
DO 52 I11=1,NFREAC , RUNKUT
FTERM(I11) = FRATE(I11)*Y(LL1(I11)) , RUNKUT
FTERM(I11+NFREAC) = FTERM(I11) , RUNKUT
52 CONTINUE , RUNKUT
JRKX = (JRK-1)*NSPEC , RUNKUT
DO 70 M2=3,NSPEC , RUNKUT
MJRK = JRKX+M2 , RUNKUT
IIX = (M2-3)*NREAC , RUNKUT
DY = 0.0 , RUNKUT

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NNSTOP = NTERM(M2)
DO 60 NN=1,NNSTOP
  IF (NASRAS(IIIX+NN) .LE. NREAC) GO TO 55
  DY = DY+TERM(NASRAS(IIIX+NN))
  GO TO 60
55 DY = DY - TERM(NASRAS(IIIX+NN))
60 CONTINUE
  IIFX = (M2-3)*NFREAC
  NFSTOP = NTERM(M2)
  DO 65 NF=1,NFSTOP
    IF (NUSRUS(IIFX+NF) .LE. NFREAC) GO TO 63
    DY = DY + FTERM(NUSRUS(IIFX+NF))
    GO TO 65
63 DY = DY - FTERM(NUSRUS(IIFX+NF))
65 CONTINUE
  KRK(MJRK) = DY
70 CONTINUE
  DO 80 M3=3,NSPEC
    MJRK = JRKX+M3
    XXRK = ARK(JRK)*(KRK(MJRK)-BRK(JRK)*QRK(M3))
    Y(M3) = Y(M3) + H*XXRK
    QRK(M3) = QRK(M3)+3.0*XXRK-CRK(JRK)*KRK(MJRK)
80 CONTINUE
90 CONTINUE
  K5MAX = 0.01
  DO 100 M4=3,NSPEC
    IF (Y(M4) .LT. 0.0) Y(M4) = 0.0
    IF (ABS(KRK(M4)+NSPEC)) .LT. 1.0E-10 .OR.
1  ABS(1.0-KRK(M4)/KRK(NSPEC+M4)) .LT. 1.0E-2 .OR.
2  ABS(KRK(M4)+KRK(NSPEC+M4)+KRK(2*NSPEC+M4)+KRK(3*NSPEC+M4))*H
3  .LT. YOLD(M4)*1.0E-4) GO TO 100
  K5 = ABS((KRK(NSPEC+M4)-KRK(2*NSPEC+M4))/(KRK(M4)-KRK(NSPEC+M4)))
  IF (K5 .GT. K5MAX) K5MAX = K5
100 CONTINUE
  IF (K5MAX .LT. 0.10) GO TO 120
  H = H*0.08/K5MAX
  IFLAG2 = 0
  DO 110 M5=2,NSPEC
    Y(M5) = YOLD(M5)
    QRK(M5) = QOLD(M5)
110 CONTINUE
  GO TO 40
120 T = T+H
  H = H*0.08/K5MAX
  HCOUNT = HCOUNT+1
  IF (IFLAG2 .EQ. 0) GO TO 10
  CALL R9EXUN
  RETURN
END

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SUBROUTINE WEIRD
COMMON /A/      A(51)          ,ARK(4)          ,B(51)          ,WEIRD
1 BRK(4)         ,CRK(4)         ,F(20)          ,FF(20)         ,WEIRD
2 FLUX(120)      ,FLXINF(120)    ,FRATE(20)     ,FTERM(40)     ,WEIRD
3 FTERMW(40)     ,G(20)          ,GG(20)         ,HBAR(20)      ,WEIRD
4 H2HOLD(20)     ,H3HOLD(20)    ,IATOM(10,20)   ,IGAIN(4)      ,WEIRD
5 IGAINA(20,20)  ,IGAINB(20,20)  ,IGAINC(20,20)  ,IGAIND(20,20) ,WEIRD
6 ILOSS(4)       ,ILOSSA(20,20)  ,ILOSSB(20,20)  ,ILOSSC(20,20) ,WEIRD
7 ILOSSD(20,20)  ,INFORM(30)     ,JPULL(20)      ,K(1000)       ,WEIRD
8 K0(51)         ,KABS(20,120)   ,KABS2(120)     ,KABS02(120)   ,WEIRD
9 KABS03(120)    ,KRK(80)        ,L1(51)         ,L2(51)        ,WEIRD
X L3(51)         ,LL1(21)        ,LL2(21)        ,LL3(21)       ,WEIRD
1 N(51)          ,NASRAS(1000)   ,NFTERM(20)     ,NTERM(20)     ,WEIRD
2 NUSRU(400)     ,PHOLD(20,20)   ,PROHLD(71,20)  ,QOLD(20)      ,WEIRD
3 GRK(20)        ,R1(51)         ,R2(51)         ,R3(51)        ,WEIRD
4 RR1(21)        ,RR2(21)        ,RR3(21)        ,SUMIN(10,20)  ,WEIRD
5 TAB02(87)      ,TAB03(87)      ,TEMP(20)       ,TERM(100)     ,WEIRD
6 TERMW(100)     ,Y(20)          ,YHOLD(20,20)   ,YLAST(20,20)  ,WEIRD
7 YNEW(20)       ,YOLD(20)       ,YPRINT(20,20)  ,YSTART(20,20) ,WEIRD
8 Y3SUN(20)      ,Y4SUN(20)     ,Z(20)          ,ZPRINT(20)    ,WEIRD
COMMON /B/      ALPHA, EQUIL, H, HCOUNT, IFLAG1, IFLAG2, WEIRD
2 IFLAG3, IFLAG4, IFLAG5, IFLAG6, IFLAG7, IFLAG8, WEIRD
3 IFLAG9, IJZX, ITCHXX, IUNIT, JCNTRL, JFLAG2, WEIRD
4 JFLAG6, JOSHUA, JZEND, JZMAIN, LAT, LONG, WEIRD
5 NFREAC, NREAC, NSPEC, PI, T, TDAY, WEIRD
6 THOUR, TMAX1, TMAX2, TMIN, TMONTH, TOLD, WEIRD
7 TPRINT, TQUIT, TSEC, ZBOTUM, ZSTEP, ZTOP WEIRD
INTEGER HCOUNT,PHOLD,R1,R2,R3,RR1,RR2,RR3,RX1,RX2,RX3, WEIRD
1 TMONTH,TDAY,THOUR,TMIN,TSEC,TX WEIRD
REAL KO,N,KABS,K,KRK,LAT,LONG,K5,K5MAX,KABS02,KABS03,KABS2 WEIRD
AKRACY = 1.0E-3 WEIRD
HMIN = 1.0E-6 WEIRD
YNEW(1) = 1.0 WEIRD
CALL Q9EXUN WEIRD
H = HBAR(JZMAIN)*3.0 WEIRD
IF (H .LT. TPRINT-(T-TOLD)) GO TO 10 WEIRD
H = TPRINT-(T-TOLD) WEIRD
IFLAG2 = 1 WEIRD
10 DO 100 I1=1,NREAC WEIRD
TERM(I1) = K(I1*JZEND-IJZX)*Y(L1(I1))*Y(L2(I1))*Y(L3(I1)) WEIRD
TERM(I1+NREAC) = TERM(I1) WEIRD
100 CONTINUE WEIRD
DO 200 I11=1,NFREAC WEIRD
FTERM(I11) = FRATE(I11)*Y(LL1(I11)) WEIRD
FTERM(I11+NFREAC) = FTERM(I11) WEIRD
200 CONTINUE WEIRD
DO 500 M1=3,NSPEC WEIRD
F(M1) = 0.0 WEIRD
G(M1) = 0.0 WEIRD
NNSTOP = NTERM(M1) WEIRD
IIIX = (M1-3)*NREAC WEIRD
DO 300 NN=1,NNSTOP WEIRD
NASX = NASRAS(IIIX+NN) WEIRD
IF (NASX .GT. NREAC) GO TO 250 WEIRD

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      G(M1) = G(M1) + TERM(NASX)
      GO TO 300
250 F(M1) = F(M1) + TERM(NASX)
300 CONTINUE
      IIFX = (M1-3)*NFREAC
      NFSTOP = NFTERM(M1)
      DO 400 NF=1,NFSTOP
      NUSX = NUSRUS(IIFX+NFX)
      IF (NUSX .GT. NFREAC) GO TO 350
      G(M1) = G(M1) + FTERM(NUSX)
      GO TO 400
350 F(M1) = F(M1) + FTERM(NUSX)
400 CONTINUE
      IF (Y(M1) .LT. 1.0E-100) GO TO 450
      G(M1) = G(M1)/Y(M1)
      GO TO 500
450 G(M1) = 0.0
500 CONTINUE
600 DO 700 M2=3,NSPEC
      IF (G(M2) .LT. 1.0E-100 .AND. F(M2) .LT. 1.0E-100) GO TO 675
      IF (G(M2)*H .LT. 1.0E-8) GO TO 675
      IF (G(M2)*Y(M2)*1.0E8 .LT. F(M2)) GO TO 650
      IF (F(M2)*1.0E8 .LT. G(M2)*Y(M2)) GO TO 625
      YNEW(M2) = (Y(M2)-F(M2)/G(M2))*EXP(-G(M2)*H) + F(M2)/G(M2)
      GO TO 700
625 YNEW(M2) = Y(M2)*EXP(-G(M2)*H)
      GO TO 700
650 YNEW(M2) = Y(M2) + F(M2)*H
      GO TO 700
675 YNEW(M2) = Y(M2)
700 CONTINUE
      DO 800 I2=1,NREAC
      TERMW(I2)=K(I2*JZEND-IJZX)*YNEW(L1(I2))*YNEW(L2(I2))*YNEW(L3(I2))
      TERMW(I2+NREAC) = TERMW(I2)
800 CONTINUE
      DO 900 I12=1,NFREAC
      FTERMW(I12) = FRATE(I12)*YNEW(LL1(I12))
      FTERMW(I12+NFREAC) = FTERMW(I12)
900 CONTINUE
      DO 1200 M3=3,NSPEC
      FF(M3) = 0.0
      GG(M3) = 0.0
      NNSTOP = NTERM(M3)
      I11X = (M3-3)*NREAC
      DO 1000 NN2=1,NNSTOP
      NASX = NASRAS(I11X+NN2)
      IF (NASX .GT. NREAC) GO TO 950
      GG(M3) = GG(M3) + TERMW(NASX)
      GO TO 1000
950 FF(M3) = FF(M3) + TERMW(NASX)
1000 CONTINUE
      I1FX = (M3-3)*NFREAC
      NFSTOP = NFTERM(M3)
      DO 1100 NF2=1,NFSTOP

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NUSX = NUSRUS1 IFX=NF2)
IF (NUSX .GT. NFREAC) GO TO 1050
GG(M3) = GG(M3) + FTERMW(NUSX)
GO TO 1100
1050 FF(M3) = FF(M3) + FTERMW(NUSX)
1100 CONTINUE
IF (YNEW(M3) .LT. 1.0E-100) GO TO 1150
GG(M3) = GG(M3)/YNEW(M3)
GO TO 1200
1150 GG(M3) = 0.0
1200 CONTINUE
DELMAX = 0.0
DO 1400 M4=3,NSPEC
IF (Y(M4) .LT. 1.0E-100) GO TO 1400
IF (ABS(Y(M4)*G(M4)-F(M4))*EXP(-G(M4)*H)*1.0E2 .LT. F(M4))
1 GO TO 1400
IF (GG(M4)*H .GT. 300.0) GO TO 1400
IF (GG(M4) .LT. 1.0E-100 .AND. FF(M4) .LT. 1.0E-100) GO TO 1275
IF (GG(M4)*H .LT. 1.0E-8) GO TO 1275
IF (GG(M4)*YNEW(M4)*1.0E8 .LT. FF(M4)) GO TO 1250
IF (FF(M4)*1.0E8 .LT. GG(M4)*YNEW(M4)) GO TO 1225
YBACK = (YNEW(M4)-FF(M4)/GG(M4))*EXP(-GG(M4)*H)+FF(M4)/GG(M4)
GO TO 1300
1225 YBACK = YNEW(M4)*EXP(GG(M4)*H)
GO TO 1300
1250 YBACK = YNEW(M4) - FF(M4)*H
GO TO 1300
1275 YBACK = YNEW(M4)
1300 DEL = ABS(YBACK/Y(M4) - 1.0)
IF (DEL .GT. DELMAX) DELMAX = DEL
1400 CONTINUE
IF (DELMAX .LE. AKRACY) GO TO 1500
IF (H .LT. 1.01*HMIN) GO TO 1500
H = H/2.0
IF (H .LT. HMIN) H = HMIN
IFLAG2 = 0
GO TO 600
1500 DO 1700 M6=3,NSPEC
FBAR = (F(M6)+FF(M6))/2.0
GBAR = (G(M6)+GG(M6))/2.0
IF (GBAR .LT. 1.0E-100 .AND. FBAR .LT. 1.0E-100) GO TO 1575
IF (GBAR*H .LT. 1.0E-8) GO TO 1575
IF (GBAR*Y(M6)*1.0E8 .LT. FBAR) GO TO 1550
IF (FBAR*1.0E8 .LT. GBAR*Y(M6)) GO TO 1525
Y(M6) = (Y(M6)-FBAR/GBAR)*EXP(-GBAR*H) + FBAR/GBAR
GO TO 1700
1525 Y(M6) = Y(M6)*EXP(-GBAR*H)
GO TO 1700
1550 Y(M6) = Y(M6) + FBAR*H
GO TO 1700
1575 Y(M6) = Y(M6)
1700 CONTINUE
T = T+H
HCOUNT = HCOUNT + 1

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IF (IFLAG2 .EQ. 1) GO TO 9000	WEIRD
IF (DELMAX .GT. 1.0E-8) GO TO 1800	WEIRD
H = H*1.0E2	WEIRD
GO TO 1900	WEIRD
1800 H = H*1.5	WEIRD
IF (H .LT. HMIN) H = HMIN	WEIRD
1900 IF (H .LT. TPRINT - (T-TOLD)) GO TO 10	WEIRD
H = TPRINT - (T-TOLD)	WEIRD
IFLAG2 = 1	WEIRD
GO TO 10	WEIRD
9000 CALL R9EXUN	WEIRD
RETURN	WEIRD
END	WEIRD
SCOPE	
LOAD	

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SUBROUTINE MICROPLT
COMMON /A/ A(51) , ARK(4) , B(51) , MICROPLT
1 BRK(4) , CRK(4) , F(20) , FF(20) , MICROPLT
2 FLUX(120) , FLXINF(120) , FRATE(20) , FTERM(40) , MICROPLT
3 FTERMW(40) , G(20) , GG(20) , HBAR(20) , MICROPLT
4 H2HOLD(20) , H3HOLD(20) , IATOM(10,20) , IGA(4) , MICROPLT
5 IGA(20,20) , IGA(20,20) , IGA(20,20) , IGA(20,20) , MICROPLT
6 ILOSS(4) , ILOSSA(20,20) , ILOSSB(20,20) , ILOSSC(20,20) , MICROPLT
7 ILOSSD(20,20) , INFORM(30) , JPULL(20) , K(1000) , MICROPLT
8 K0(51) , KABS(20,120) , KABS2(120) , KABS2(120) , MICROPLT
9 KABS3(120) , KRK(80) , L1(51) , L2(51) , MICROPLT
X L3(51) , LL1(21) , LL2(21) , LL3(21) , MICROPLT
1 N(51) , NASRAS(1000) , NFTERM(20) , NTERM(20) , MICROPLT
2 NUSRUS(400) , PHOLD(20,20) , PROHLD(71,20) , GOLD(20) , MICROPLT
3 QRK(20) , R1(51) , R2(51) , R3(51) , MICROPLT
4 RR1(21) , RR2(21) , RR3(21) , SUMIN(10,20) , MICROPLT
5 TAB02(87) , TAB03(87) , TEMP(20) , TERM(100) , MICROPLT
6 TERMW(100) , Y(20) , YHOLD(20,20) , YLAST(20,20) , MICROPLT
7 YNEW(20) , YOLD(20) , YPRINT(20,20) , YSTART(20,20) , MICROPLT
8 Y3SUN(20) , Y4SUN(20) , Z(20) , ZPRINT(20) , MICROPLT
COMMON /B/ ALPHA , EQUIL , H , HCOUNT , IFLAG1 , IFLAG2 , MICROPLT
2 IFLAG3 , IFLAG4 , IFLAG5 , IFLAG6 , IFLAG7 , IFLAG8 , MICROPLT
3 IFLAG9 , IJZX , ICHXX , IUNIT , JCNTRL , JFLAG2 , MICROPLT
4 JFLAG6 , JOSHUA , JZEND , JZMAIN , LAT , LONG , MICROPLT
5 NFREAC , NREAC , NSPEC , PI , T , TDAY , MICROPLT
6 THOUR , TMAX1 , TMAX2 , TMIN , TMONTH , TOLD , MICROPLT
7 TPRINT , TQUIT , TSEC , ZBOTUM , ZSTEP , ZTOP , MICROPLT
INTEGER HCOUNT , PHOLD , R1 , R2 , R3 , RR1 , RR2 , RR3 , RX1 , RX2 , RX3 , MICROPLT
1 TMONTH , TDAY , THOUR , TMIN , TSEC , TX , MICROPLT
COMMON/DD/IN , IOR , IT , IS , IC , ICC , IX , IY , MICROPLT
COMMON/DDID/ID(4) , IFL , LU , MICROPLT
DATA(ID=32HG W ADAMS X=3918,MICROPLT ) , MICROPLT
DIMENSION TEXT1(10) , TEXTV(2) , IXHOLD(20,20) , MICROPLT
DATA(TEXTV=16H HEIGHT(KM) ) , (NCYCLE=0) , MICROPLT
IFL = IFL+1 , MICROPLT
MINY=20*(INT(Z(JZEND)))/20 , MICROPLT
MAXY=20*(INT(Z(1)-1)/20+1) , MICROPLT
NTICS=(MAXY-MINY)/10+1 , MICROPLT
IF(NCYCLE) GO TO 20 , MICROPLT
NCYCLE=1 $ MAXPOWR=0 , MICROPLT

C LOOP 100 COMPUTES RANGE OF YHOLD.
DO 100 ISPEC=3,NSPEC , MICROPLT
J=-1 , MICROPLT
10 J=J+1 $ IF(YHOLD(ISPEC,JZEND)/10.**J.GT.1) GO TO 10 , MICROPLT
100 IF(J.GT.MAXPOWR) MAXPOWR=J , MICROPLT

C LOOP 800 PLOTS UP TO 5 CURVES/FRAME
20 NOPLTS =(NSPEC+2)/5 , MICROPLT
DO 800 IPLOT=1,NOPLTS , MICROPLT
IN=IS+1 , MICROPLT
CALL DDBOX(70,1020,70,1020) , MICROPLT

C LOOP 200 DRAWS VERTICAL TICS AND HEIGHTS.

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